

ENVIRONMENT ENGINEERING

water demand :-

for an average indian town
the requirement of water in various
uses is —

domestic purpose	135 lpcd
Industrial "	40 "
Public use "	25 "
fire demand	15
losses, wastage, Theft	55 lpcd
total water demand	270 lpcd

note:-

① IS code domestic
As water demand = 135 to 225
lpcd.

② under ordinary condition

min. domestic water demand for a
town having flushing system = 200 lpcd

But for EWS & LIG colony = 135 lpcd

③ IS code max. water demand = 335 lpcd
As per

v. gnd

note: coincident draft
= max. daily demand + fire
demand

fire demand formula's

1- Kuichling formula	$2182\sqrt{P} \rightarrow (\text{lt/min})$
2- freeman "	$1136(P_{10} + 10) (\text{lt/min})$
3- Buston "	$5663\sqrt{P} (\text{lt/min})$
4- National Board of fire under writer's formula	• for $P < 2$ lakh $4637\sqrt{P} \left[1 - \frac{\sqrt{P}}{100}\right] (\text{lt/min})$ • for $P > 2$ lakh. → 54600 lt/min for 1st fire → 9100 to 36400 lt/min for 2nd fire
5. Govt. of India	$100\sqrt{P} (\text{KL})$

note: $P \rightarrow$ in thousands
(Population) Ans $\rightarrow$ lt/min
except Govt.
formula

units	Design parameter
water treatment unit	for 15 years, max. daily demand
Pipe mains, filter, other treatment unit	max. daily demand
Distribution system or distribution mains	max { ① max. hourly demand of max. day ② coincident draft
well & tubewells	max. daily demand
demand reservoir	Average annual demand
Service reservoir	15 years
Pipe connection to several treatment units, distribution system	30 years

Ex

$$\text{max. daily demand} = 1.8 (\text{Avg. daily demand})$$

$$\text{max. hourly demand} = 1.5 \times \text{Avg. hourly demand of max. day}$$

$$= 1.5 \times \left(\frac{\text{max. daily demand}}{24} \right)$$

$$= 1.5 \times 1.8 \times \left(\frac{\text{Avg. daily demand}}{24} \right)$$

$$= 2.7 \text{ Annual avg. hourly demand}$$

Ex

$$\frac{\text{max. daily demand}}{\text{Avg. daily demand}} = 1.8$$

180 %

$$\frac{\text{max. weekly demand}}{\text{Avg. weekly}} = 1.48$$

148 %

$$\frac{\text{max. monthly demand}}{\text{avg. monthly demand}} = 1.28$$

128 %

Goodrich formula ..

$$\frac{\text{Peak (max) demand}}{\text{Avg. demand}} = 180 t^{-0.1}$$

$P = \text{Percentage of annual avg. demand for time 't' in days}$

Population	Peak factor
< 50000 (small town)	3
50000 - 2 लाख (medium town)	2.5
> 2 लाख (large town)	2

Population forecasting methods :

① Arithmetical Increase method

- assumption $\rightarrow$ future population increases at constant rate $\left(\frac{dp}{dt} = k\right)$

$$P_n = P_0 + n\bar{x}$$

$\rightarrow$ no. of decades

- suited $\rightarrow$ large & established cities where there is limited scope of expansion (old cities)

② Geometric Increase method (Uniform Increase method)

- assumption $\rightarrow$ per decade % growth rate is constant

$$P_n = P_0 \left(1 + \frac{r}{100}\right)^n$$

$$r = \sqrt[n]{\frac{P_2}{P_1}} - 1$$

$$r = (r_1 r_2 \dots r_n)^{1/n}$$

- suited $\rightarrow$ Applied to young & rapidly developing cities with a large scope of expansion

③ Incremental Increase method or method of varying increment

$$P_n = P_0 + n\bar{x} + \frac{n(n+1)}{2}\bar{y}$$

$\bar{x} \rightarrow$ avg. increase of population of known decade

- suited $\rightarrow$ to any city (old or new)

$\bar{y} =$ avg. of incremental increase of known decades

④ decreasing rate of growth method

- when rate of growth shows downward trend. if population is reaching towards saturation and growth rate is decreasing

⑤ comparative graphical method

- cities of similar condition & characteristics are selected which have grown in similar fashion in the past, plotting graph & compares.

⑥ Logistic Curve method by (P.F. Verhulst)

Ex. 1931 P_0 $t_0 = 0$
 1941 P_1 $t_1 = t$
 1951 P_2 $t_2 = 2t$

$$t = \log r$$

Population at any time 't' from start

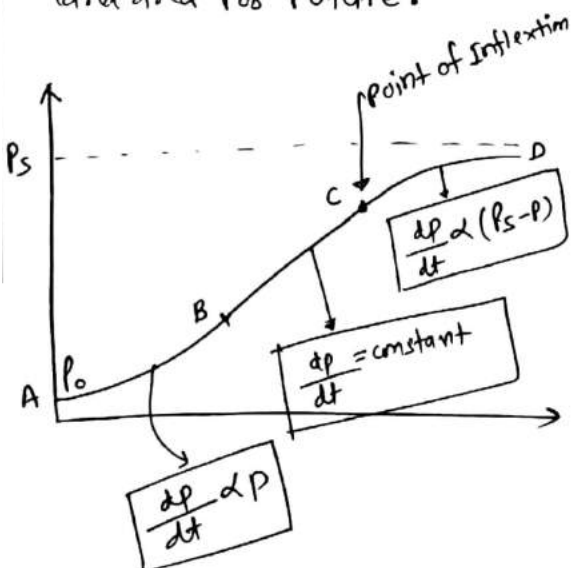
$$P = \frac{P_s}{1 + m \ln^{-1}(nt)}$$

$$m = \frac{P_s - P_0}{P_0}$$

$$P_s = \frac{2P_0P_1P_2 - P_1^2(P_0 + P_2)}{P_0P_2 - P_1^2}$$

$$n = \frac{1}{t_1} \ln \left\{ \frac{\frac{P_s - P_1}{P_1}}{\frac{P_s - P_0}{P_0}} \right\}$$

for community with limited land area for future.

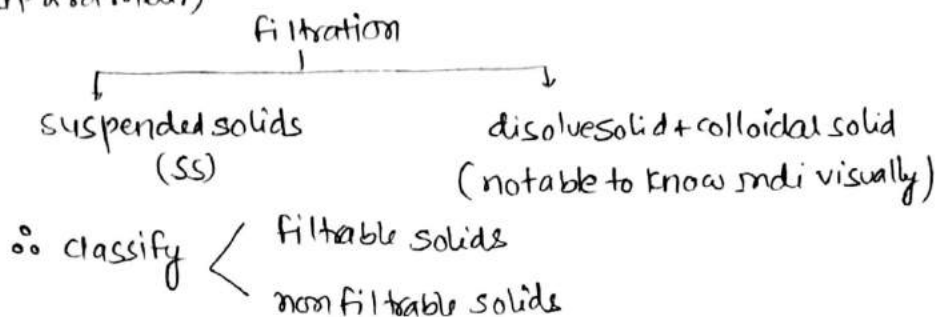


Physical parameter

① suspended solid

- origin → from inorganic particles, only in surface water (not in ground water)
- measurement → By Gravimetric technique
- dissolve solids = total solids - suspended solids
(chemical parameter)

SS > 30 mg/l
As per EPA



② Turbidity

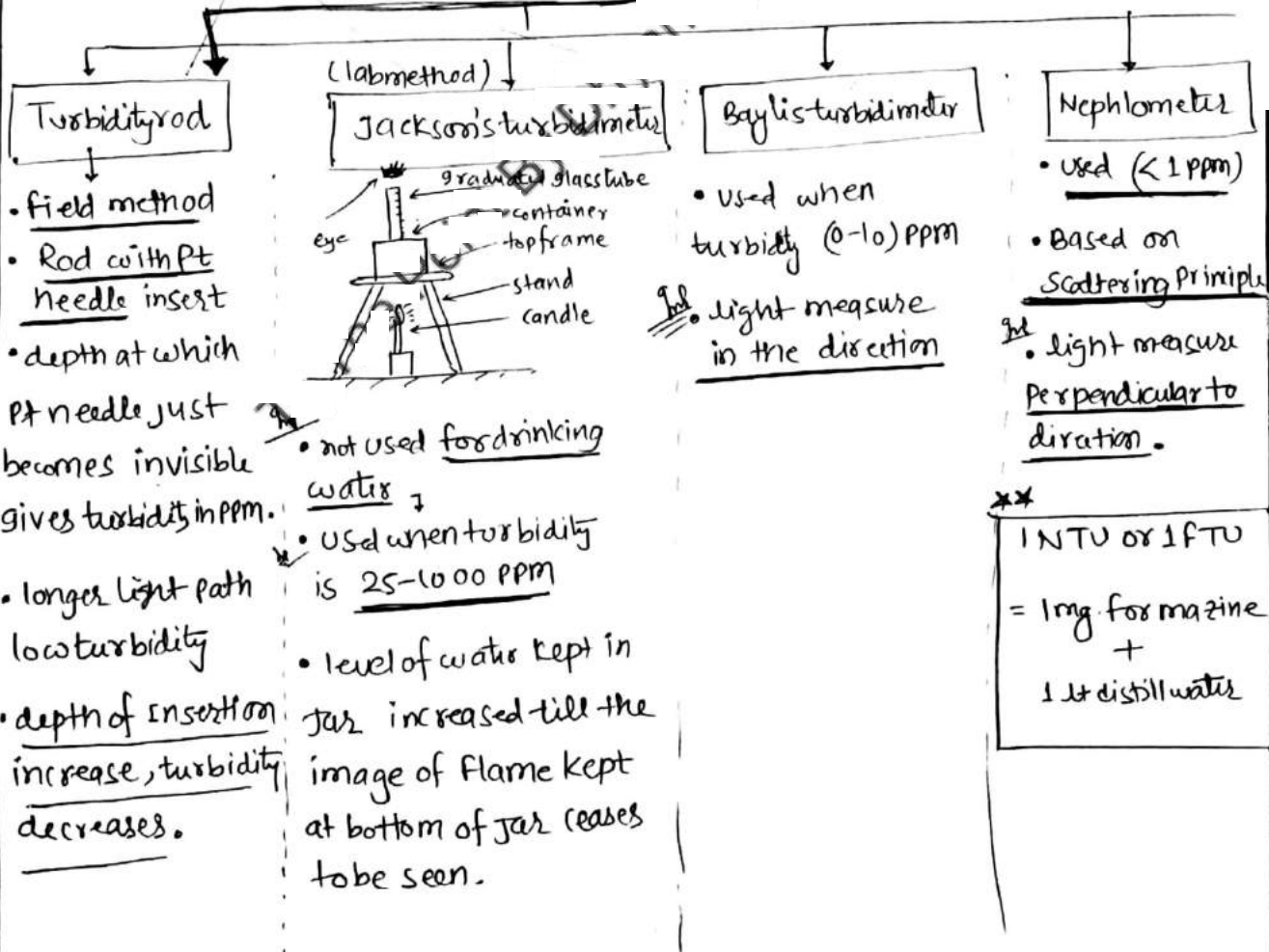
1-5 NTU

- Indirect measurement of suspended solid
- 1 standard Turbidity unit (1STU)

* 1STU = 1 mg Silica (SiO₂) + 1 litre distill water
fuller earth

absorption method

measurement



modern method to turbidity measurement

Photometer

③ color

5-15 Hazen

• origin → due to suspended & dissolved matter in water

• ^{1st} measurement → By tintometer (nessler tubes) → (color matching Technique)

— using Burgness scale, cobalt scale

• 1 True color unit / 1 hazen unit = 1mg Pt (chloroplatinic 100) + 1 litre water

note:- It is only for yellowish Brown color

note:- other than this like Industry effluent, spectrophotometric technique used ^{2nd}

④ taste, odour

(TON $\times 3$)

origin → By dissolve gases $\begin{cases} \rightarrow \text{H}_2\text{S} \\ \rightarrow \text{methane} \\ \rightarrow \text{mercaptans} \end{cases}$

measurement → By osmoscope

• Threshold odour number (TON) = $\frac{A+B}{A}$

↓
take final volume of ~~Bottle~~ = 200ml [if nothing given]

⑤ temperature

(10-25°C)

$\neq 25^\circ\text{C}$

• An increase in 10°C temp → doubles the Biological activity.

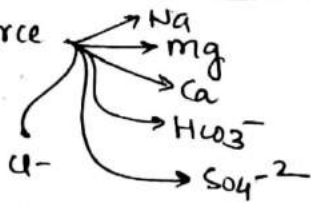
chemical water Quality Parameter

Description

① total dissolve solids (TDS)

500-2000 ppm

major source



measurement

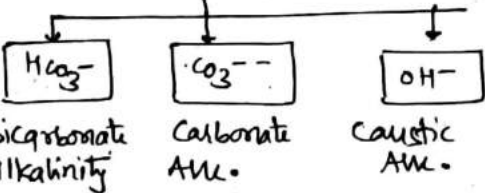
(rough)
dionic Tester

(Exact)
Gravimetric Technique

residual ion $TDS = 0.65 \times EC \left(\frac{mho/cm}{(mho/cm)} \right) @ 25^\circ C$

② Alkalinity
(200-600) mg/L

Source



• Definition → amt of ions to neutralize H^+ ions

titrant = $\frac{N}{50} H_2SO_4$

indicator ⇒ ① phenolphthaleine ② methyl orange

∴ HCO_3^- & OH^- → never exist at a time ∴ HCO_3^-, OH^-, CO_3^{--} X never at a time

③ pH
6.5-8.5

pH < 5.6 acid rain

- measurement by → "Aquascope potentiometer with calomel rods"
- Indicator → Bromine-methyl (∴ range - 6 to 7.6)

note:-

pH



Alkaline water

Corrosion & Tuberculosis

Incrustation in pipe

(deposits of minerals on interior of pipe from material being conveyed)

deposition of ferrous oxide (tubercles) from water

name	Indicator type	pH range	Initial color	Final color
① methyl orange	acidic indicator	(2.8-4.2)	Red	yellow
② Phenolphthaleine	Basic indicator	(8.6-10.3)	colorless	red
③ Br-methyl	-	(6-7.6)		

④

Hardness
(200-600)
mg/l

→ Produced by multivalent cation $\{Ca^{+2}/Mg^{+2}/Al^{+3}/Si^{+4} etc\}$
→ measurement by Spectrophotometric Technique

note:-
 $CaCO_3$ &
 $MgCO_3$
↓
least soluble

titrant $\Rightarrow$ $\frac{N}{50}$ EDTA
ethylenediamine tetraacetate

Indicator -
EBT
red $\rightarrow$ blue
initial final

types	carbonate hardness (CH) or temporary hardness	HCO_3^- & CO_3^{2-}	min (TH, Alk)
	noncarbonate hardness (NCH) or permanent hardness	$SO_4^{2-}/Cl^-/NO_3^-$ nitrate	TH - CH

note:- Zero hardness by $\rightarrow$ ion exchange method / zeolite method / Base exchange treatment

$\rightarrow$ British degree of hardness $\rightarrow$ 14.25 mg/l as $CaCO_3$
 $\rightarrow$ French $\rightarrow$ 10 " " "

⑤ chloride content as (Cl)
(250-1000)
mg/l

Mohr's method ($\frac{N}{37.5}$ $AgNO_3$, Potassium chromate ($K_2Cr_2O_4$) $\rightarrow$ Brown red ppt is formed at end of titration.

argentometric method

• sudden increase $\rightarrow$ organic pollution

note $\rightarrow$ total concentration of chlorine $\rightarrow$ By (SNORT) method (Amperometric titration)

⑥ Nitrogen content

note:-
free ammonia + organic ammonia $\Rightarrow$ Kjeldal nitrogen
if nitrate excess $\rightarrow$ Blue baby disease (methemoglobinemia) (affect health of infants)

nitrogen content and Presence of organic matter

free ammonia
(0.15 mg/l)

recent pollution
Simple Boil & measure

organic ammonia
(0.30 mg/l)

Albuminoid
quantity of nitrogen before decomposition or organic complex nature

Boiling + $KMnO_4$ (A.C. soln)

NO_2^- Nitrite
(0)

Partial decomposition condition
color match (SAW)

Sulphonic acid + naphthamine

NO_3^- Nitrate
(45) mg/l

old pollution / fully decomposed / fully oxidised
color match (P4/104)

phenoldi-sulphonic acid + potassium hydroxide

⑦ ^{gnd} Fluoride

acceptable
limit = 1 mg/Lt

rejection
limit = 1.5 mg/Lt

upto 1mg/Lt fluoride required

for growth of permanent teeth
and to prevent dental cavity

fluoride > 1.5 mg/Lt

case-1 fluoride
1.5 - 2 mg/Lt

^{gnd} mottling of teeth
(discoloration of teeth)

note → infants affects, not adult

case-2 fluoride > 5 mg/Lt

^{gnd} Bone fluorosis
& skeletal deformation
(deformation of bone)

⑧ Dissolve oxygen (DO)

measurement by winkler method for pure water

NaOH + KI

titrant = $\frac{N}{40} \text{Na}_2\text{S}_2\text{O}_3$
Sodium tetrathionate

indicator → starch

- if brown ppt. ($\text{MnO}_2 \downarrow$) $\xrightarrow{\text{H}_2\text{O}_2}$ DO present
- if white ppt. ($\text{Mn}(\text{OH})_2 \downarrow$) $\xrightarrow{\text{H}_2\text{O}_2}$ DO absent.

note:- modified winkler method (if water has ferric ion, nitrite ion)

titrant:- $\frac{N}{40} \text{Na}_2\text{S}_2\text{O}_3 + (\text{NaOH} + \text{KI} + \text{NaN}_3 \text{ (azide)})^{**}$

Indicator - starch

^{2nd}

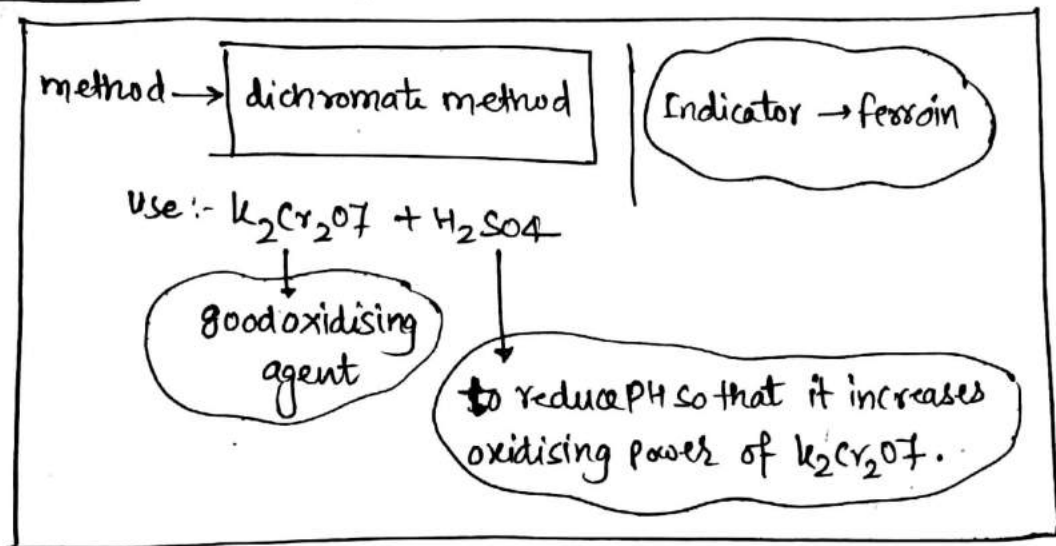
temp	Saturated DO (mg/Lt)
0°C	14.62
20°C	9.17
30°C	7.63

^{2nd} increase: effect on DO

Temperature	Solubility of gas ↓ DO ↓
chloride ion	DO ↓
Pressure	DO ↑

Some other Topics :-

① COD :-



- a sample of domestic sewage is digested with
 - Ag_2SO_4 (silver sulphate)
 - H_2SO_4 (sulphuric acid)
 - $K_2Cr_2O_7$
 - $HgSO_4$
- The digested sample is then titrated with standard ferrous ammonium sulphate (FAS) to determine unreacted amount of $K_2Cr_2O_7$.

② jar test → to know coagulant dose

Biological water quality Parameters :-

Pathogen Bacteria → difficult task to test in lab & count.

we count → presence of coliform (E-coli)
 ↓
 (harmless aerobic lactose fermenting organism)

if coliform absent → then pathogen absent

Test of coliform

membrane filtration technique

- Nutrient → M-Indormedium
- Coliform colonies counted.

MPN Test

(most probable no.)

By multiple tube fermentation test.

coliform Index Test

Reciprocal of smallest quantity of sample giving (+)ve B coli Test

Water Borne Diseases

Bacteria

- 1- Typhoid (Salmonella typhi)
- 2- Cholera (Vibrio cholera)
- 3- Bacillary dysentery (Shigella flexner, Shigella sonnei)

Virus

- 1- Jaundice (Hepatitis Virus)
- 2- Polio (Poliovirus)

Protozoa

- 1- Amoebic dysentery (Entamoeba histolytica)

MPN Test → 3 phase :-

(Based on Application of Poisson distribution)

1- Presumptive Test :- (+)ve result test indicates the likely presence of coliform.

2- Confirmed Test - sample from (+)ve tube of presumptive Test is used to confirm presence of coliform.

3- Completed Test - used for obtaining isolated colonies, cells from isolated colonies are gram stained & examined under microscope to confirm the coliform.

MPN calculation

- By MPN table
- By Thomas's eqn
- By Poisson's distribution formula

Thomas's eqn :-

$$\text{MPN} = \frac{\text{no. of (+)ve tube} \times 100}{\text{ml of sample in (-)ve tube} \times \text{ml of sample of all tubes}}$$

Nuisance bacteria

Iron (Fe-bacteria)

Pitting and tuberculation in pipe

unsuitable for industrial purpose.

Sulphur-Bacteria

durability affected

acid produced during their metabolism is destructive to concrete & other structure hence durability affected.

V. Imp.

AS per IS: 10500 Latest version - 2012 for Drinking water :-

Water quality Parameter

Permissible limit

Cause for rejection

Physical

Suspended solids

500

2000 mg/Lt

turbidity

1

5 NTU

color

5

15 hazen

(2n)

taste & odour

1

3 TON

temp

10-25°C

10-25 otherwise reject

total dissolved solids

500

2000 mg/Lt

Alkalinity

200

600 mg/Lt

hardness

200

600 mg/Lt

pH

(6.5-8.5)

(6.5-8.5) otherwise reject

chloride content (as Cl⁻)

250

1000 mg/Lt

free ammonia

0.15

0.15 mg/Lt

organic ammonia

0.30

0.30 mg/Lt

nitrite

0

0

Nitrate

45 mg/Lt

45 mg/Lt

Sulphates (SO₄-2)

200

400 mg/Lt

fluoride

1

1.5 mg/Lt

free residual chlorine

0.2

1 mg/Lt

Iron (Fe)

0.3

no relaxation (0.3) mg/Lt

Manganese (Mn)

0.1

0.3 mg/Lt

Copper

0.05

1.5 mg/Lt

Calcium (Ca)

75

200 mg/Lt

Zn (Zinc)

5

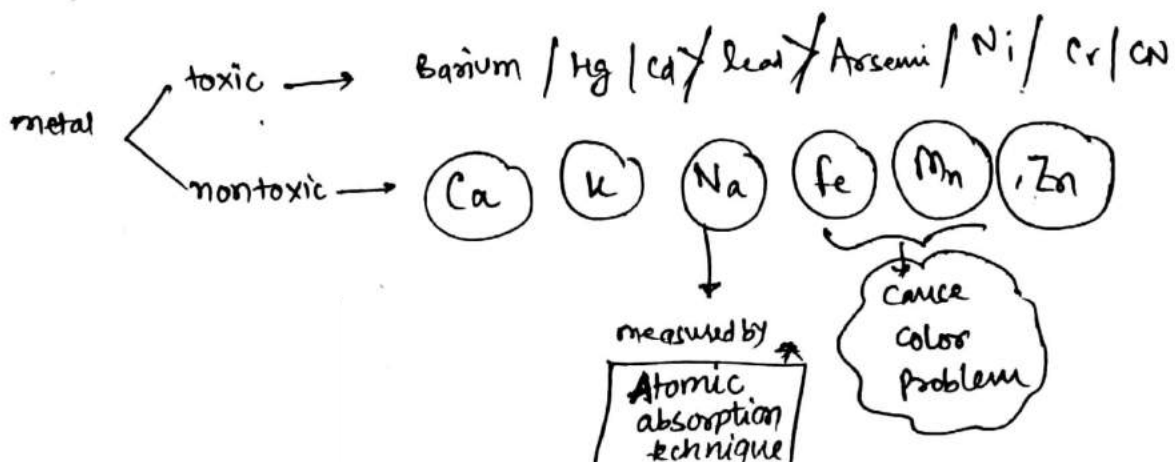
15 mg/Lt

metals

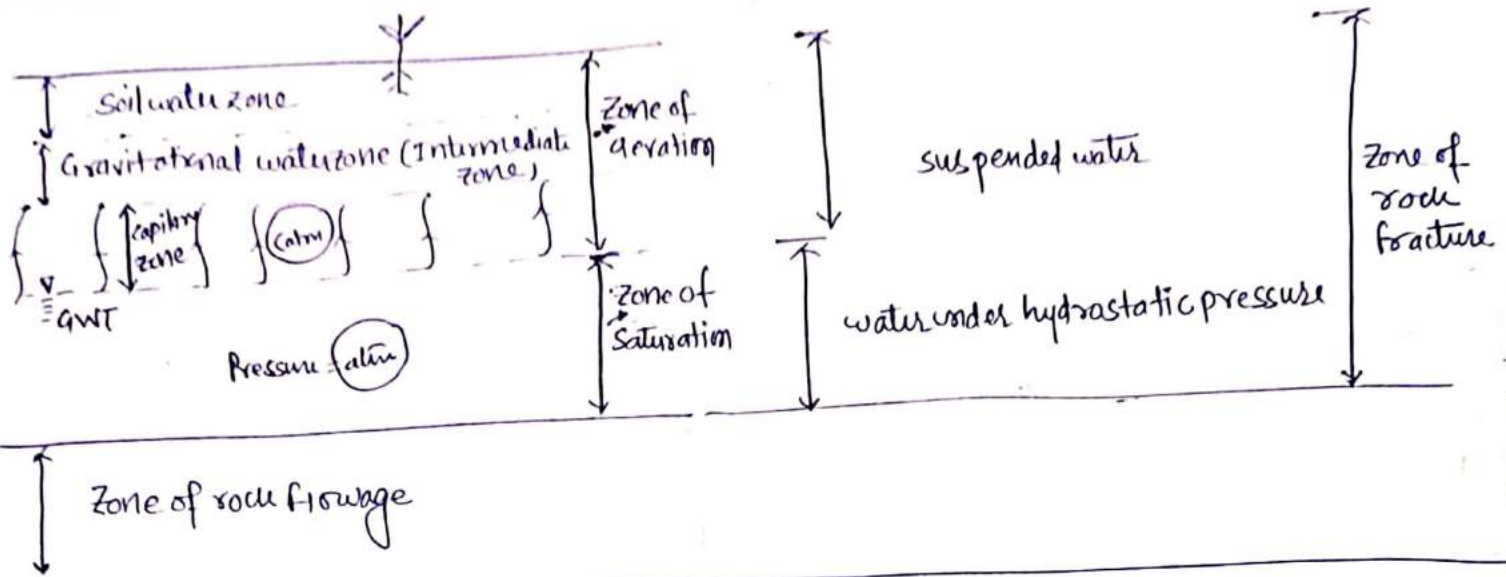
long respiratory problem

dangerous metal order :-
(सबसे खतरनाक)

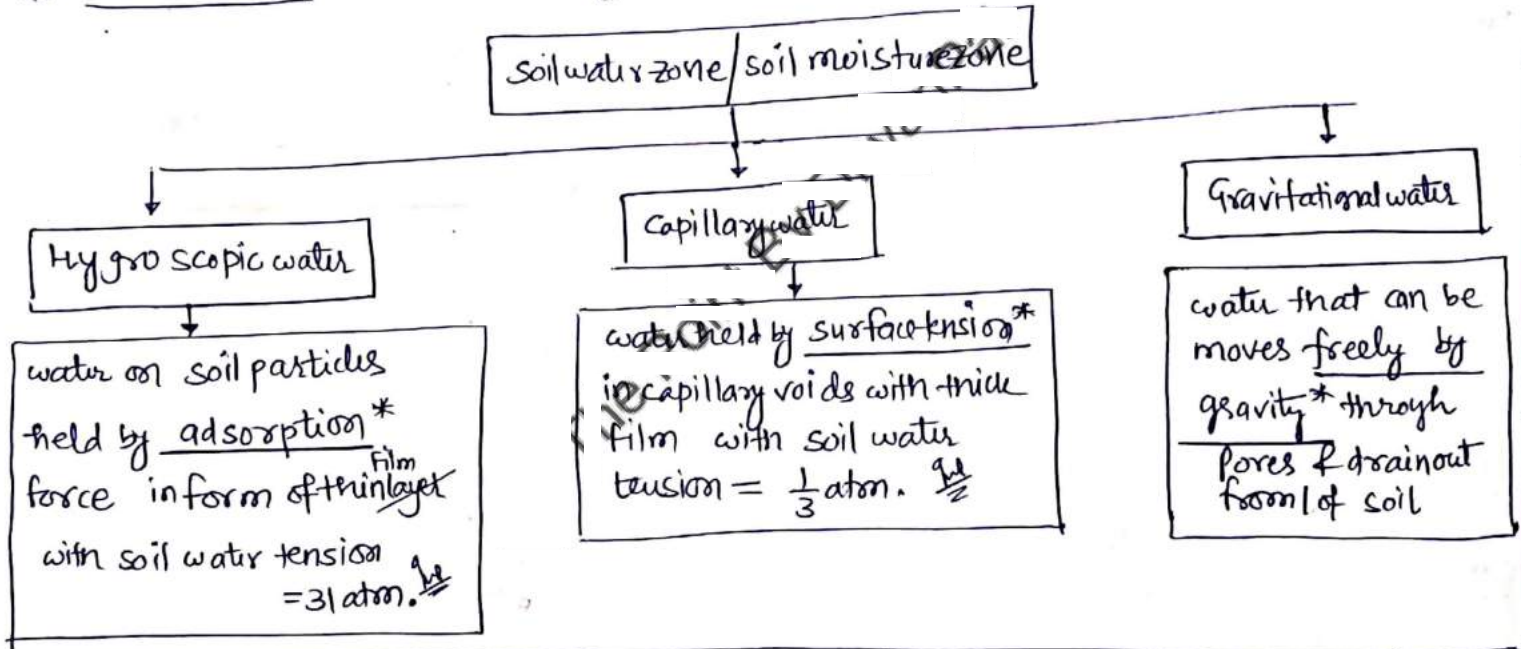
Hg > Cd > lead > Arsenic > Ni > Cr & CN
भारकरी Pb



Development of gnd. water



① soil water zone :- water drawn by vegetation, unsaturated except period of heavy infiltration.



② Intermediate zone → above capillary zone, all infiltration water must pass through it.

③ Capillary zone →

- above zone of saturation.
- Pressure < atm. pressure (101.3 KPa)
- unsaturated zone (partially zone)

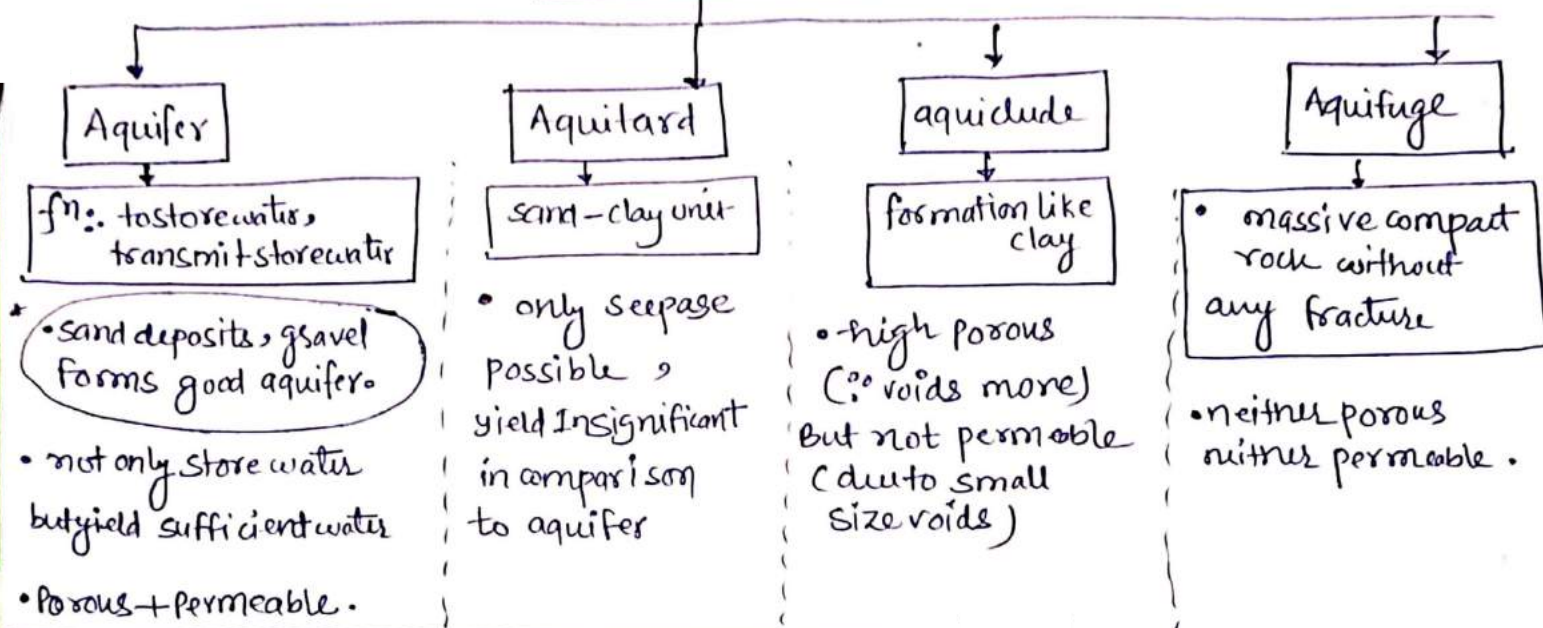
$$h = \frac{4T \cos \theta}{\rho g r}$$

④ zone of saturation →

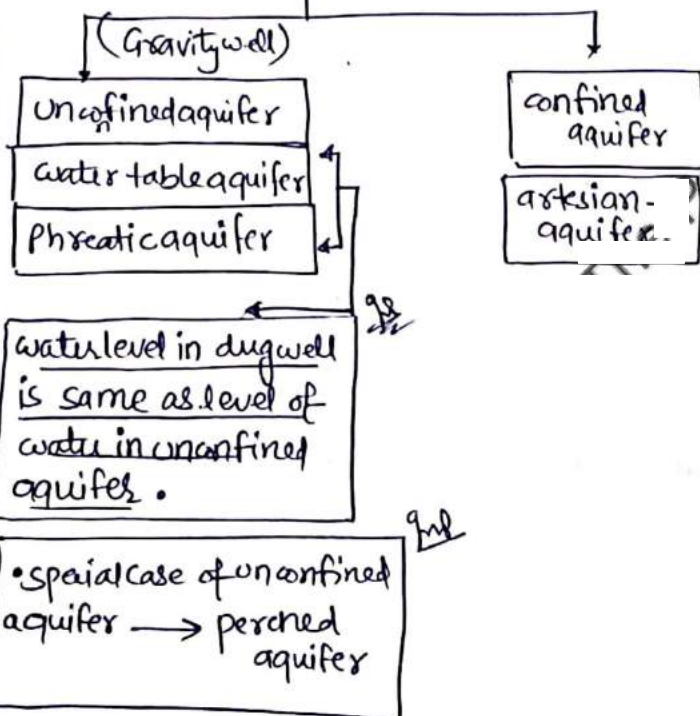
- below ground water table (GWT)
- pores completely filled by water
- Pressure = atm. pressure

from ground water utilization →

Saturated formation



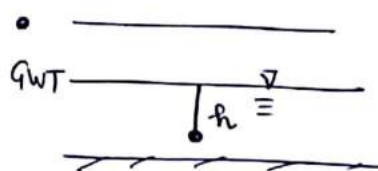
Aquifer



① unconfined / water table / phreatic aquifer :

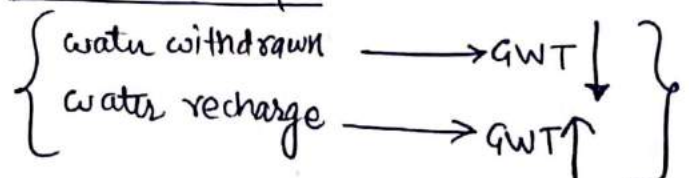
• in this gravity well exists

• absence of layer (above GWT) confining zone of saturation
→ ∴ unconfined aquifer.

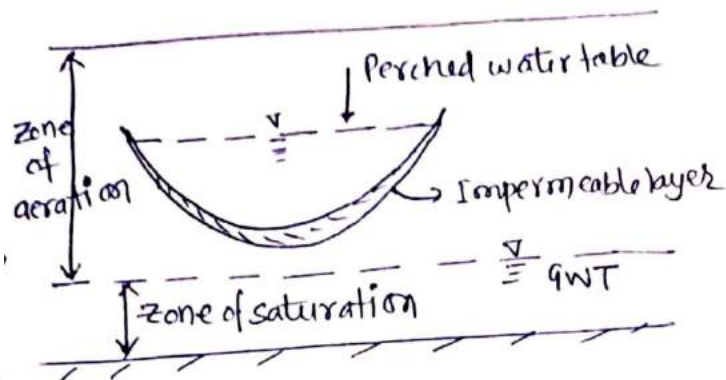


hydraulic head at any point in unconfined aquifer
= h = depth of point below GWT

• in unconfined aq.

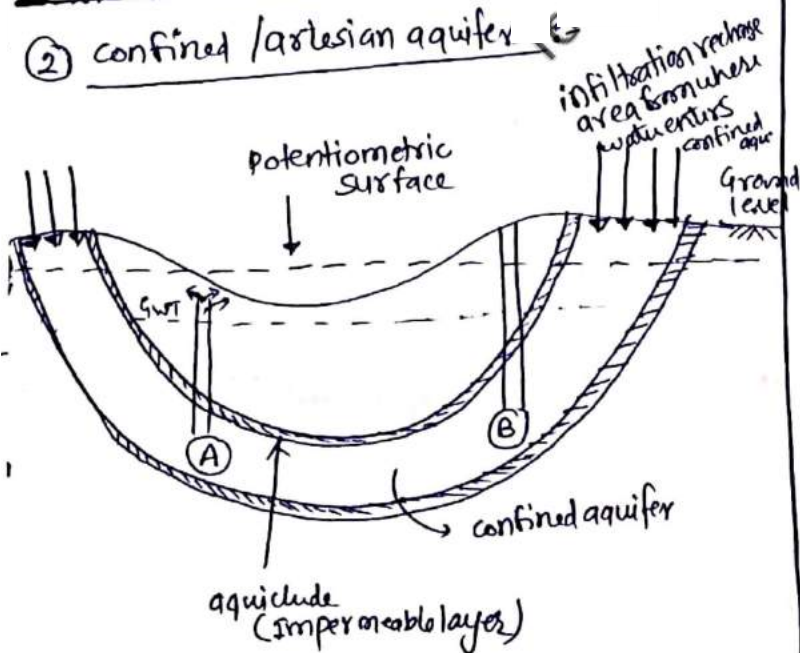


special case of unconfined aquifer
→ perched aquifer :-



- perched aquifer → above GWT exist
- ↓
- Infiltrated rainwater intercepted by Impermeable layer & local zone of saturation formed. upper surface of zone is perched water table.

② confined / artesian aquifer →



① → flowing well → when grd. level is below potentiometric surface

② → non flowing well → when grd. level is above of Potentiometric surface.

Potentiometric surface :-

- level upto which water will rise in the well
- Indicates magnitude of pressure within confined area.

• confined aquifer overlain by aquiclude (Impermeable layer)

• confined aquifer not directly contact with atmosphere.

↓

• Ground water within confined aquifer
Pressure > atm. pressure
↓
artesian pressure or confined pressure

• well dug in confined aquifer

→ water rises in well, due to release of pressure within - confined aquifer.

Some Important Definitions :-

① Porosity (n) = $\frac{V_v}{V}$

↓
volume of porous medium or aquifer material.

② specific yield (S_y) :- actual volume of water that can be extracted by gravity from unit-volume of aquifer material (porous medium)

③ specific retention S_R :- fraction of water held back in aquifer per unit volume of aquifer material.

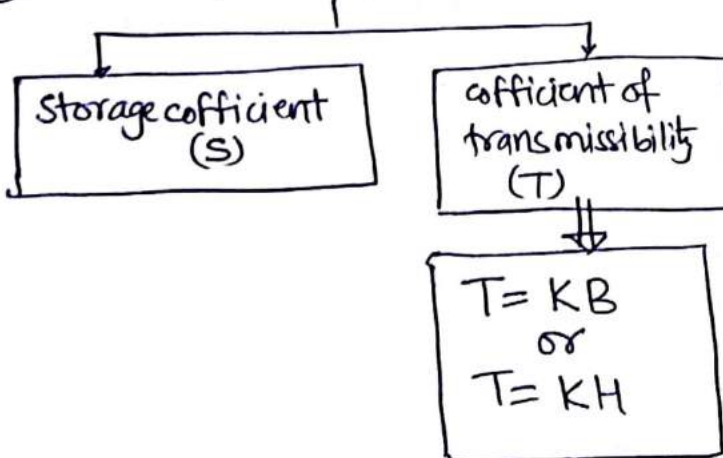
$\frac{V_{WR}}{V}$

note:- for unconfined aquifer :-

$$S_y + S_R = n \quad \text{Porosity}$$

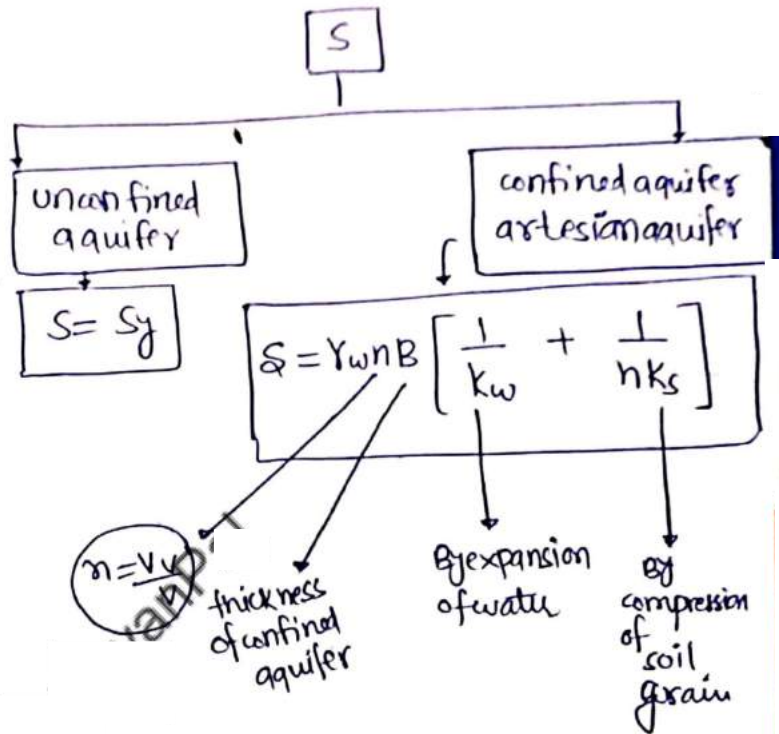
$$\frac{V_{WY}}{V} + \frac{V_{WR}}{V}$$

④ formation coefficient



⑤ storage coefficient (S) :-

• volume of water given by unit plan area of aquifer when piezometric surface falls by unity. Ind



note:

Storage coefficient due to expansion of water (%) =

$$= \frac{YwnB \left[\frac{1}{k_w} \right] \times 100}{YwnB \left[\frac{1}{k_w} + \frac{1}{nk_s} \right]}$$

⑥

$$\text{Specific storage (Ss)} = \frac{\text{Storage coefficient (S)}}{\text{Depth of confined (B) aquifer}}$$

- Solely due to compression of aquifer and expansion of water

True
UP

equation of motion

True
(CS)

for unconfined aquifer

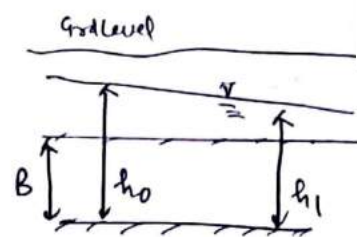
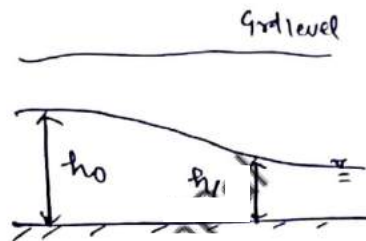
for confined aquifer

HGL (water surface) → parabola

HGL → straight line

⑦

$$\text{specific capacity} = \frac{\text{discharge}}{\text{drawdown}}$$



$$q = \frac{k(h_0^2 - h_1^2)}{2L}$$

$$q = \frac{kB(h_0 - h_1)}{L}$$

(per unit width)

⑧

Intrinsic / specific permeability :-

unit = m² or darcy

$$\Rightarrow \frac{kA}{\gamma_w}$$

Independent of Fluid Property

$$1 \text{ darcy} = 10^{-15} \text{ m}^2$$

Pumping In Test

→ for smaller area

Open end Test

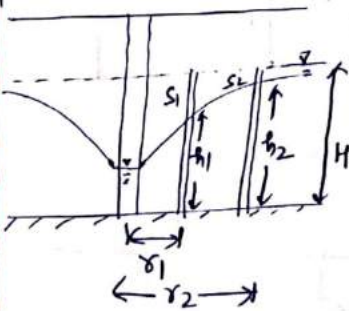
Packer Test

Pumping out Test

→ for large area

for unconfined aquifer

(Dupit's theory)



$$R = 3000 S \sqrt{k}$$

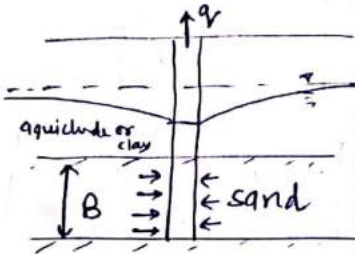
(Radius of influence)

$$k = \frac{2.303 q \log\left(\frac{r_2}{r_1}\right)}{\pi(h_2^2 - h_1^2)}$$

→ dupit

$$k = \frac{2.303 q \log\left(\frac{r_2}{r_1}\right)}{2\pi B(h_2 - h_1)}$$

$$2\pi B(h_2 - h_1)$$



Drawback in dupit's & Theim's theory

→ to achieve equilibrium condition pumping done for long time so that steady flow can be maintained, which is not easy to do.

So adopt nonequilibrium formula

for confined aquifer

(or) unsteady radial flow in confined aquifer

$$\text{well function} = W(u) = \int_u^\infty \frac{e^{-u}}{u} dt$$

$$W(u) = \ln \frac{4Tt}{r^2 S} - 0.5772$$

$$W(u) = \ln \frac{2.25 Tt}{r^2 S}$$

→ coeff. of transmissibility

→ Storage coeff.

→ radius of observation well from pumping well

drawdown in well after 't' time →

$$s = \frac{Q}{4\pi T} \times \text{well fn}$$

$$s_2 - s_1 = \frac{Q}{4\pi T} \ln\left(\frac{t_2}{t_1}\right)$$

note:- originally for unconfined flow, eqn is given by dupit, later modified by theim for confined flow.

well loss in confined aquifer

total drawdown in well S_w

formation loss
 $C_1 Q$

+

well loss
 $C_2 Q^2$

head loss required
to cause laminar
flow in porous
media.

$S_w \propto Q^2$

$S_w \propto Q^2$

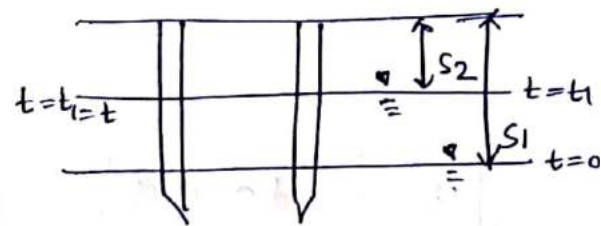
drop of
Piezometric
head required
to sustain
turbulent flow
near well

head loss
in casing
and
screen.

$$\text{well efficiency} = \frac{\text{formation loss } (C_1 Q)}{\text{total drawdown measured in well } (C_1 Q + C_2 Q^2)}$$

$$\text{specific capacity} = \frac{\text{discharge } (Q)}{\text{drawdown } (S_w)} = \frac{Q}{C_1 Q + C_2 Q^2}$$

openwell Recuperation Test :-



$$Q = S A \left(\frac{C}{A_1} \right)$$

depression head

well area
 $\left(\frac{\pi d^2}{4} \right)$

$\frac{C}{A_1}$ = specific capacity of open well
or specific yield

$$\frac{C}{A_1} = \frac{2.303}{T} \log \frac{S_1}{S_2}$$

S_1 → Initial drawdown
at $t=0$

S_2 → final drawdown
at $t=T$

Interference among wells

Q individual of well ↓
But Q total ↑

unconfined aquifer

$$Q = Q_1 + Q_2$$

$$Q = Q_1 + Q_2 + Q_3$$

confined aquifer

2 wells :-

$$Q_1 = Q_2 = \frac{\pi K (H^2 - h^2)}{2.303 \log\left(\frac{R}{r} * \left(\frac{R}{D}\right)\right)}$$

$R \rightarrow$ Radius of area of influence
 $D \rightarrow$ distance between wells

3 wells $\rightarrow$ in form of equilateral triangle
Identical

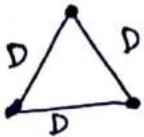
$$Q_1 = Q_2 = Q_3 = \frac{\pi K (H^2 - h^2)}{2.303 \log\left(\frac{R}{r} * \left(\frac{R}{D}\right) * \left(\frac{R}{D}\right)\right)}$$

2 wells :-

$$Q_1 = Q_2 = \frac{2\pi KB (H - h)}{2.303 \log\left(\frac{R}{r} * \left(\frac{R}{D}\right)\right)}$$

3 wells identical $\rightarrow$ in form of equilateral triangle

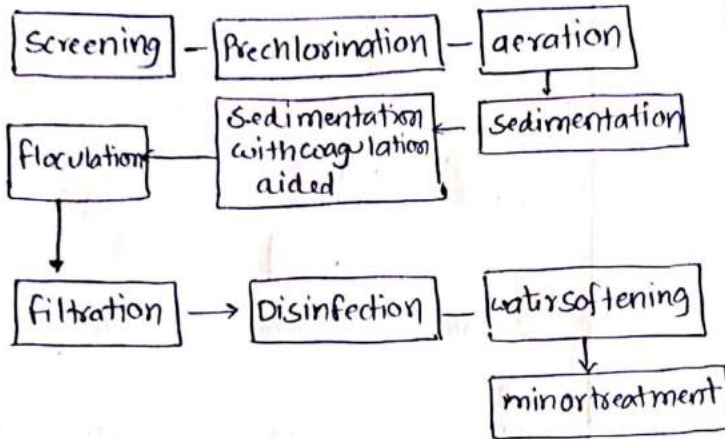
$$Q_1 = Q_2 = Q_3 = \frac{2\pi KB (H - h)}{2.303 \log\left(\frac{R}{r} * \left(\frac{R}{D}\right) * \left(\frac{R}{D}\right)\right)}$$



* Water Treatment :-

treatment based on $\left\{ \begin{array}{l} \text{in water quality} \\ \text{output we want} \\ \text{(treated water)} \end{array} \right.$

Water treatment process flowchart :-



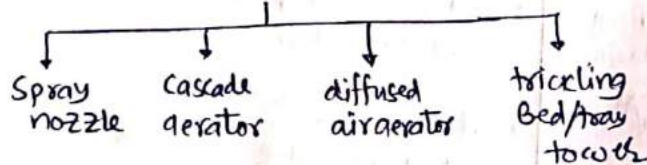
1- screening $\left\{ \begin{array}{l} \text{coarse screens} \\ \text{fine screens} \end{array} \right.$

2 Prechlorination :- when extremely polluted clear water or there is bacteria, then only add Cl_2 .

3- aeration :- add O_2 for oxidation of undesirable substance like oil, decomposing product of Algae.

- remove dissolve gases $\left\{ \begin{array}{l} \text{CO}_2 \\ \text{H}_2\text{S} \end{array} \right.$
- remove $\left\{ \begin{array}{l} \text{color} \\ \text{taste} \\ \text{odour} \end{array} \right. \rightarrow \text{remove Fe, Mn}$

methods



• note: - Dissolve oxygen $\uparrow \Rightarrow$ acidity $\uparrow =$ corrosion $\uparrow$

④ Sedimentation : $\{ \rightarrow \text{remove suspended solids by gravity action} \}$

Sedimentation tank

Quiescent type
or fill & draw type
or Intermittent type

detention time $t_d = 24 \text{ hr}$
min no = 3 (1 standb)

continuous type

Horizontal type

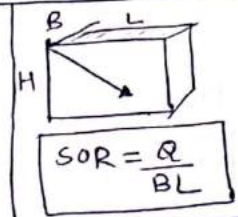
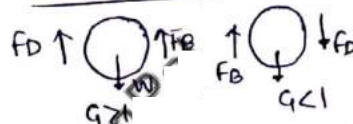
Ex: Rectangular

vertical type

Ex: circular

note: min no. of tank based on detention time (t_d)
may $\rightarrow$ discharge Q

Stoke's law



$$V_s = \left[\frac{4}{3} \frac{(G-1)gd}{C_D} \right], \quad C_D = \frac{24}{Re} \quad Re < 0.5$$

$$C_D = \frac{24}{Re} + \frac{3}{\sqrt{Re}} + 0.34 \quad 0.5 < Re < 10^4$$

$$C_D = 0.44 \quad Re > 10^4$$

V. Imp

$$V_s = \frac{(G-1) \gamma_w d^2}{18 \mu} \quad \left\{ T = 20^\circ\text{C}, d < 0.1 \text{ mm} \right\}$$

$$V_s = \frac{418 (G-1) d^2 (3T+70)}{100} \quad T \neq 20^\circ\text{C}, d < 0.1 \text{ mm}$$

$$V_s = 418 (G-1) d \left(\frac{3T+70}{100} \right) \quad 0.1 < d < 1 \text{ mm}$$

$$V_s = 1.8 \sqrt{g d (G-1)} \quad d > 1 \text{ mm}$$

$$t_d = \frac{L}{V_s} = \frac{H}{V_s} \rightarrow V_s$$

circular tank

$$t_d = \frac{d^2 (0.011d + 0.785H)}{Q}$$

V. V. Imp
note:

$$\begin{array}{ll} V_s \propto d^2 & d < 0.1 \text{ mm} \\ V_s \propto d & d (0.1 - 1 \text{ mm}) \\ V_s \propto \sqrt{d} & d > 1 \text{ mm} \end{array}$$

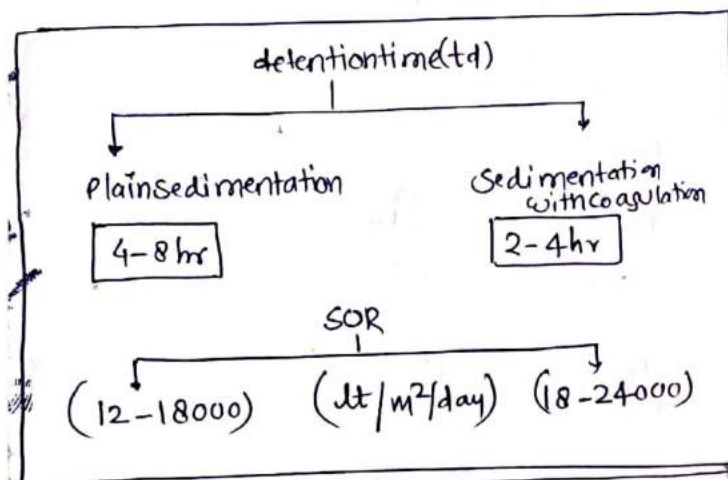
- SOR $\uparrow$ η $\downarrow$ | SOR decide efficiency of tank

$$\eta = \frac{VS}{V_0(SOR)} \times 100$$

$$\text{Settle concentration} = \text{total} - \text{removed conc.} \left(\frac{VS \times 100}{V_0} \right)$$

$$\text{displacement efficiency} = \frac{\text{Flow through period (F)}}{\text{detention period (D)}}$$

(due to current produced by coming fluid (short circuiting) $F < D$)



- ⑤ coagulation aided sedimentation
- $f_n \rightarrow$ to remove fine suspended solids
 - coagulant dose $\rightarrow$ by Jar Test

Coagulation $\rightarrow$ process of adding chemicals in water to destabilize the surface - charge of colloid particles so that free contact b/w them can take place.

mechanism of coagulation :-

- 1- Ionic layer compression
- 2- adsorption & charge neutralization
- 3- Sweep coagulation
- 4- Inter particle Bridging.

Coagulant	Description
Alum $Al_2(SO_4)_3 \cdot 18H_2O$ Aluminium Sulphate (6.5-8.3) range PH	- Commonly used dose (10-30 mg/L) - Flocus formed are <u>stable</u> - Reduce color, taste, odour. $Al_2(SO_4)_3 \cdot 18H_2O + 3Ca(HCO_3)_2$ 666 486 (162x3) $\downarrow$ $3CaSO_4 + 2Al(OH)_3 + 6CO_2 \uparrow + 18H_2O$ (Permanent hardness) (ppt. gelatine) 2x78=156 corrosion $\uparrow$ PH $\downarrow$ $\therefore Ca(HCO_3)_2$ utilization $\rightarrow$ hence decrease Alkalinity. $\text{CaO} + CO_2 \rightarrow CaCO_3 \xrightarrow[H_2O]{CO_2} Ca(HCO_3)_2$ (56) (100) (162) quick lime if Alkalinity not sufficient add lime {gives no acidity} Alum + $Ca(OH)_2$ $\rightarrow 3CaSO_4 + 2Al(OH)_3 + 18H_2O$ Permanent hardness add soda ash {gives acidity} Alum + Na_2CO_3 $\rightarrow 3Na_2SO_4 + 2Al(OH)_3 + 3CO_2 \uparrow + 18H_2O$ acidity
Copperas $(FeSO_4 \cdot 7H_2O)$ (22.5-25) range PH	- Commonly used for <u>treating sewage</u>. - Heavy flocks - PH range > 8.5
chlorinated copperas $Fe_2SO_4 + FeCl_3$	- not for colored water - effective in color removal also - works in large PH range - for low PH water treatment. - They are effective in combination with lime.
Sodium Aluminate $(Na_2Al_2O_4)$	- costly coagulant - beside coagulation, <u>reduces hardness</u> (zero hardness water can be got) - useful for water which don't require alkalinity.

Mixing Basin ::

rapid mix $T = 60 \text{ sec}$

$G_T \rightarrow$ measure of coagulation opportunity

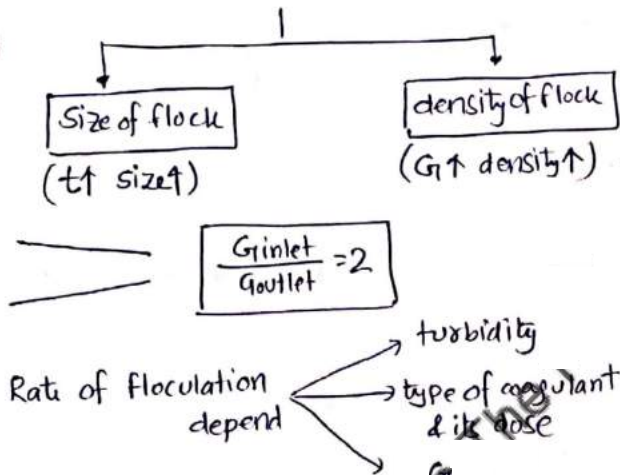
$$G = \frac{V_2 - V_1}{x} \Rightarrow \text{measure of relative velocity of 2 particles of fluid \& distance between them.}$$

(sec⁻¹)

$$G = \sqrt{\frac{P}{\mu V}} \quad \text{--- (W)} \quad \text{--- (m/s)} \quad \text{--- (N/m}^2)$$

$G \rightarrow$ temporal mean velocity gradient

⑤ Floculation :: coagulation opportunity $\uparrow \uparrow$

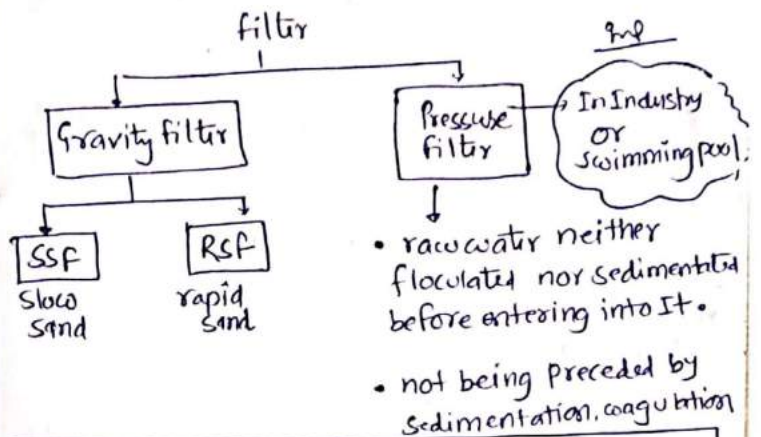


Def.

note :: clarifloculators = floculation + sedimentation
in inner tank in outer tank

⑦ Filtration :: remove

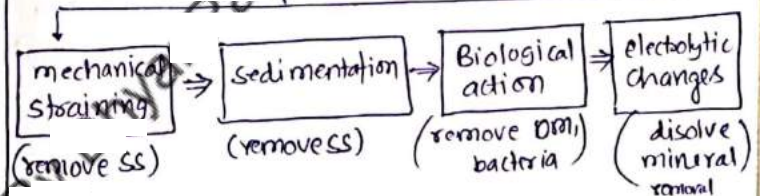
- flock particles
- color
- microorganism
- fine suspended solids particles



Roughing (dual media filter)

$\rightarrow$ increases filtration rate Ex. RSF + SSF

Theory of filtration

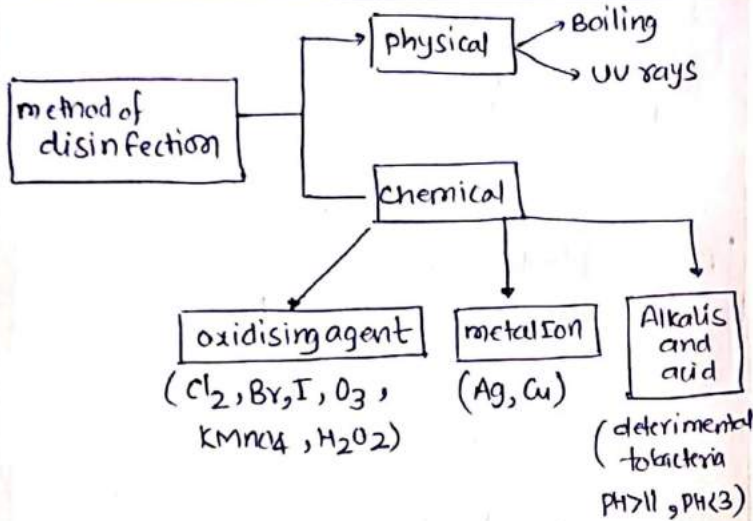


slow sand filter (SSF)	Rapid sand filter (RSF)
Operation cost low :: no other energy source required.	
Rate of filtration = 100-200 lt/hr/m ²	+ 30 times of SSF (3000-6000) lt/hr/m ²
D ₁₀ 0.20 - 0.30 2 < Cu < 3	D ₁₀ 0.35 - 0.55 1.3 < Cu < 1.7
• not use after coagulation aided sedimentation otherwise flock will clog it.	• very efficient in color removal
frequency of cleaning = 1-3 month	$N = 1.22 \sqrt{q \mu_{mb}}$ $N_{min} = 2$
Bacteria removal = 98-99%	$(1-n)D = (1-ne)De$ if expansion = 50% $\therefore De = 1.5D$
can not use if turbidity > 50 ppm	$ne = \left(\frac{V_b}{V_s}\right)^{0.22}$
remove: taste, odor (due to OM) color removal (less efficiency)	$n_L = D(1-n)(G-1)$
area > 1200 m ² min 6 unit (5+1)	<u>Problems in RSF operation</u> :: ① air binding ② Mud Ball formation ③ cracking of sand bed ④ Bumping of filter bed.

⑧ Disinfection : process of removal of disease causing micro-organism (harmful) Bacteria

• Sterilization → process of removal of all types of microorganism.

{ (doing disinfection does not mean sterilization is done) }



1- UV rays : not for turbid water (10-15 ppm)

2- O₃ : removes color, taste, odour also

- gives highest quality water
- does not ensure safety against recontamination

3- KMnO₄ : used in rural area

- 100% cholera causing bacteria removal.
- produce dark brown precipitate on utensils
- if pink color disappear means OM present

Recarbonation : most common process to reduce pH. (6.5-8.5)

- CaCO₃ ppt soluble by passing CO₂ for less load on filter.

Chick Watson law : $C^nt = \text{constant}$ { for a particular disinfection $\frac{N}{N_0} = \text{const.}$ }

$\log \frac{N_0}{N} = 1$ one log disinfection

$\log \frac{N_0}{N} = 2$ 2 log disinfection

chlorination : By this pathogens killed

- process of adding chlorine (Cl₂) or hypochlorite ion to water
- used to prevent the spread of water borne disease
 - cholera
 - dysentery
 - typhoid

Types of chlorination :

① Plain chlorination : → only chlorination & no other treatment given to water.

- remove bacteria, OM, color
- dose ⇒ 0.5 mg/l
- used when turbidity (20-30 mg/l)

② Prechlorination : in this chlorine is added before filtration or rather before sedimentation & coagulation.

- used when concentration of pathogenic bacteria is higher.

③ Superchlorination (Excess chlorination) :

- whenever excess chlorine (5-15 mg/l) is added in water during epidemic such that

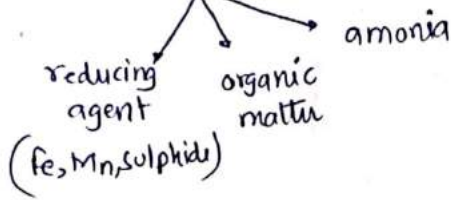
its excess residual > 1 to 2 mg/l above breakpoint chlorination)

④ Break point chlorination :-

dose = demand + residual

• Break point is a point at which the chlorine demand has been totally satisfied.

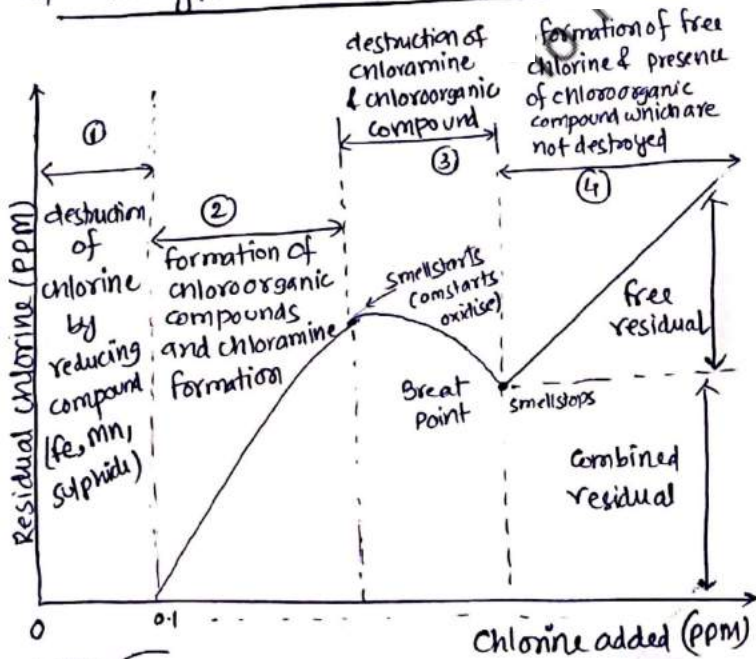
(Chlorine has reacted with in water.



• After this point whatever chlorine is added breaks free from it and appears as a residual chlorine hence this point is referred as break point.

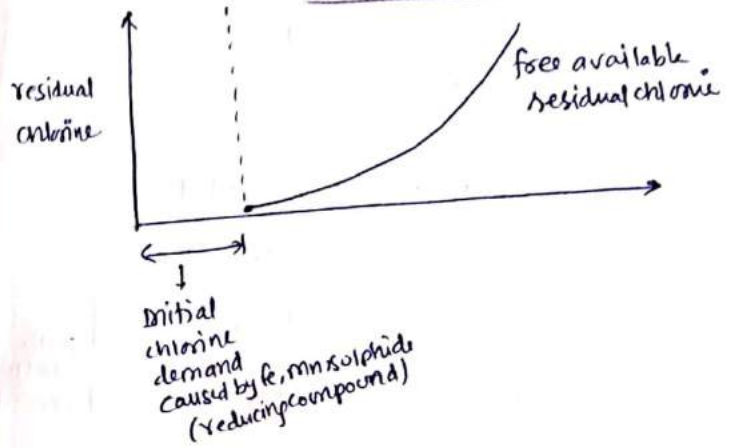
• The amount of Cl_2 required to reach upto this point is referred as break point dose.

• Theoretically no chlorine is req. to be added beyond break point but practically it is added to ensure residual chlorine of 0.2 mg/l at contact period of 10 min.



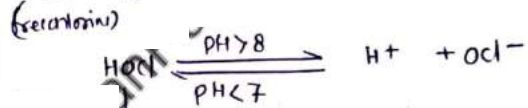
Initial chlorine demand caused due to Fe, Mn, sulphide

special case :- when no amonia or organics are present in water.

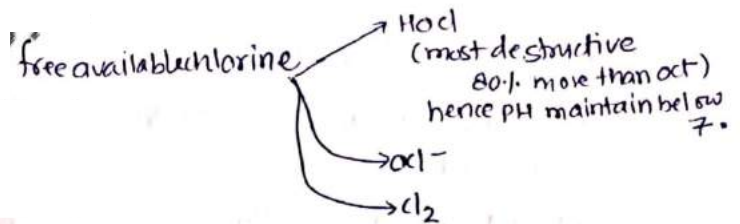


Reaction / theory behind chlorination :-

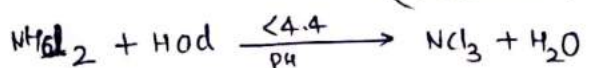
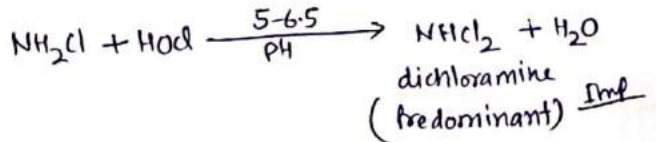
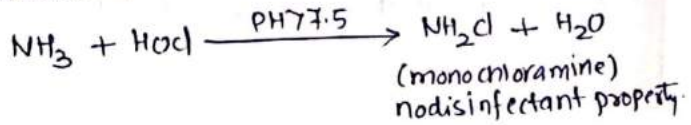
chlorination Best pH range → 5 to 7



(unstable hence breakdown at high pH)



note:- moreover chlorine will immediately react with amonia present in water to form chloramines.



note: ∵ pH maintained 5 to 7 hence

dichloramine ($NHCl_2$) Predominant.

Imp

Chloramine combined form of chlorine
less effective than free chlorine (25 times less)
But they are stable and remains in water for great duration.

forms in which chlorine is added :-

- (i) as free chlorine (gas or liquid form)
 - (ii) as Hypochlorite (Bleaching powder)
 - (iii) chloramines (amonia + chlorine)
 - (iv) chlorine dioxide ClO_2
- } no sludge formed

residual chlorine Tests :-

- (i) ortholodine Test → measure combined & free chlorine
- (ii) DPD Test
- (iii) chlorotex Test
- (iv) Starch Iodine Test

Imp

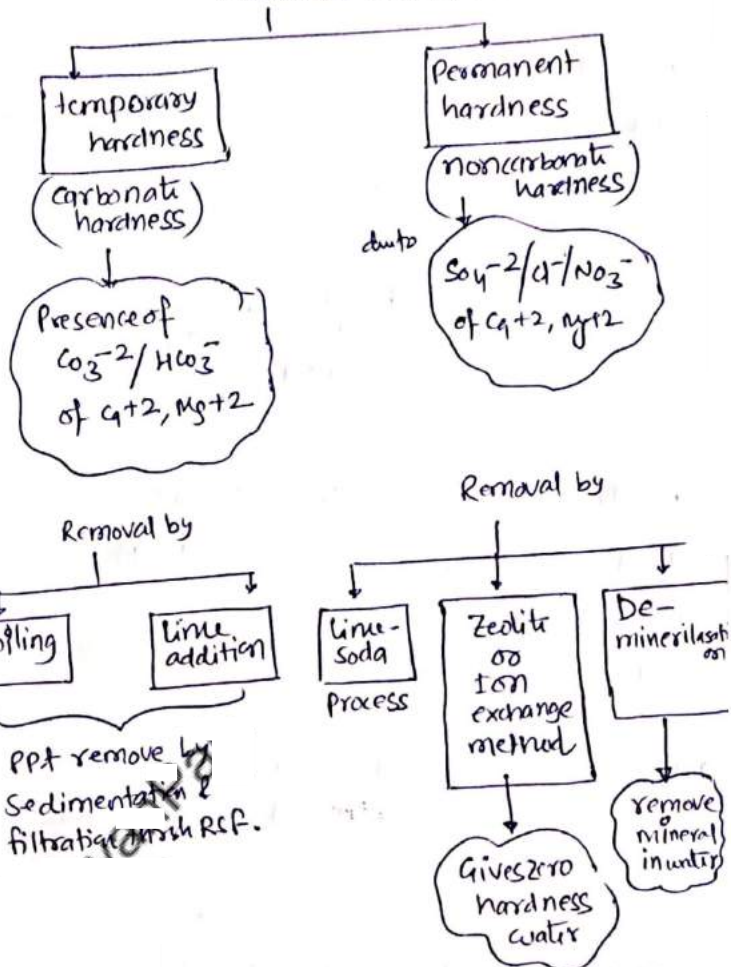
Dechlorinating agent / process :-

- 1- $Na_2S_2O_3$ (sodium thio sulphate)
cheapest
- 2- Activated carbon → costly
- 3- SO_2
- 4- UV (solar radiation)
- 5- Reverse osmosis
- 6- evaporation, freezing, electrolysis.

(3) water softening :-

$Ca^{+2}/Mg^{+2}/Fe^{+2}/Mn^{+2}/Al^{+3}$

Hardness (due to multivalent cation)



(b) minor Treatments :-

①

Activated carbon

remove taste odour color

good adsorbent
due to its
high surface
area to volume
ratio
Size 0.1-2mm

- remove Phenol type impurity.
- dechlorinating agent
- add before or after coagulation
But before ~~filtration~~ filtration.

② $\text{CuSO}_4 \rightarrow$ Kill algae.

③ Removal of Fe, Mn

without organic matter

aeration $\rightarrow$ sedimentation
filtration

combine with
organic
matter

- water ~~is added~~ to
Break bond with
 $\text{LiOH} / \text{d}_2 / \text{KMnO}_4$

④

Fluoridation (addition of Fluorine)

NaF

(Sodium
fluoride)

Na_2SiF_6

Sodium
Silico-
fluoride

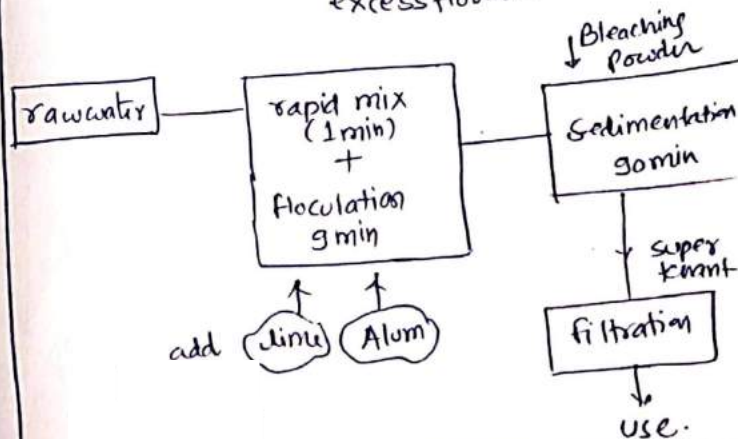
H_2SiF_6

Hexafluoro-
silicic
acid

(5) Defluoridation (Excess fluorine removal) :-

- 1- Absorption by activated Alumina { Prashanti Technology }
- 2- nalgonda Technique
- 3 - ion exchange adsorption method
- 4 - reverse osmosis process.

nalgonda Technique :- mainly used in rural areas
where ground water contains
excess fluoride.



⑥ Desalination :-

- By Reverse osmosis
- By electrolysis
- By Freezing

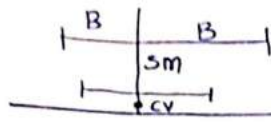
⑦ removal of toxic metals :-

(By coagulation added sedimentation)

Hyd
21/3/2020

Layout of distribution system

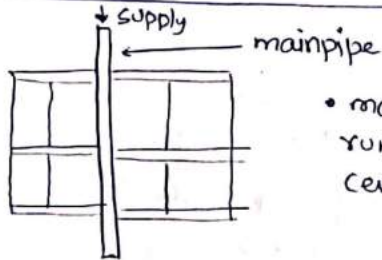
dead end system



B → Branch
sm → submain
CV → cut off valve

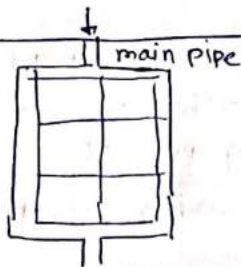
- followed for old town where houses are situated in unplanned way
- water reaches by only 1 route → disadvantage.

Grid Iron System



• main pipe run through centre.

- branch & lateral run in grid pattern which are interconnected.
- since main, branch, lateral are interconnected hence dead end eliminated and water reaching at different location by more than 1 route.

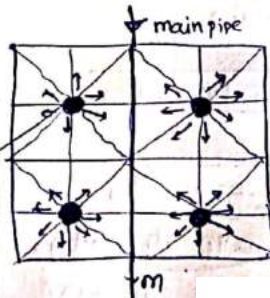


• main pipe all around the area.

Ring System or circular system

Radial system

• in this water flows towards the outer periphery.



• A big area is divided in several zone and at the centre of each zone a distribution reservoir is kept

- This method gives higher service head and efficient water distribution.

distribution reservoir

Pipe Appurtenances

1) Sluice valve or Gate valve or Shutoff valve

f^n → to regulate flow

- essential to divide the mainline into section
- provided at summit ($\because$ pressure $\rightarrow$ low)
- made of Iron with Brass mounting

not:- stopcocks (small size sluice valve)

Solid wedge type double disk type

2) Air-relief valve or air valve

• provided at summit on d/s of sluice valve to release air pressure.

(otherwise due to accumulation of air, a backward pressure is generated which cause Blockage of flow of water)

3) Check valve or reflux valve or non return valve

• allows water only in one direction.

• made by brass or gun metal

• provided in pipeline which draws water from pump

4) Scur Valve or Blowoff valve or drain valve

• provided at dead end of pipeline

f^n → to remove sand, silt from pipeline (It is similar to sluice valve but f^n different)

5) Pressure relief valve or relief valve or safety valve

• Automatic works **

• used to control/limit the pressure in system (otherwise bursting or Instrument fails)

6) Foot valve

• provided at end of pump suction pipe

f^n → to prevent entry of debris into pumping system and backflow also

7) Butterfly valve

• provided in large diameter size pipe.

• High head loss than sluice valve
 $\therefore$ not suitable for continuous Throttling/regulation (कम-वोल्ट)

8) Ball valve or Ball float valve

f^n → maintain constant level in service reservoir.

⑨ Globe Valve 	change direction through 90 degree twice $\rightarrow \therefore$ high head loss	Pipes	Description
⑩ needle cone valve	for throttling flow (regulation purpose)	cast Iron pipe	- not for pressure $> 700 \text{ kN/m}^2$ - used:- water supply for trunk + distribution system
⑪ Ball Pilot valve	- human operated - used in critical Application (emergency + safety control) (high pressure or high flow feed)	Steel pipe	- where water pressure $\rightarrow$ High & size $\rightarrow$ large (not to withstand external load of backfill or traffic)
⑫ Bibcocks	- Small size watertap $\left\{ \begin{array}{l} \text{washbasin} \\ \text{bathroom} \end{array} \right.$ - sun metal/plastic	wrought Iron	- Inside Building $\rightarrow$ service connection - easy workability - for protection against corrosion $\rightarrow$ galvanizing (zinc coating)

~~note~~ $\therefore$ GI pipe $\rightarrow$ liable to affect by acidic or alkaline water

Pressure pipe metal pipe - cast Iron - steel - wrought Iron - copper - lead - Brass non metal pipe - RCC - Prestress - asbestos - plastic - PVC - poly-ethylene - glass reinforced plastic
--

Joints in water supply pipes :-

Spigot & socket joint	Plain end → spigot end enlarge end → socket • mostly used for <u>cast Iron, steel pipes</u> this joint used.
collar joint	• <u>RCC pipe</u>, asbestos cement pipe में
expansion joint	• <u>in metal pipe</u> (to account change in pipe length) (thermal variation)
Flange joint	• <u>for temporary work</u> (where we dismantle pipeline / shifted) CI/steel • <u>not used where deflection, vibration comes</u>
flexible joint	• <u>where settlement of pipe may occur.</u>
Threaded joint	• <u>GI pipes</u>
simplex joint	in <u>asbestos pipe</u> • pipe sleeves + rubber gasket

laying of sewer :

from their outfall ends
(towards starting end)

Reason $\rightarrow$ utilization during initial period of construction
(not wait for completion of entire scheme)

Steps of laying of sewer :

① mark alignment (By theodolite + Invariantape)

Referential line method

ref. line
centreline

Sight-rail method

② Trench excavation ③ Bracing of trench

④ dewatering of trench ⑤ lay & join pipes

⑥ Testing of Leakage in sewers

By water Test

• Carried out b/w 2 manhole

By air Test

• for large dia. sewer
• measure pressure, if drops then leakage

note: apply soap solution to get exact location of leakage.

Sewer design $\rightarrow$ not design for full flow
{ Reserve space for fluctuations in Sewage flow }

Sanitary sewage $\Rightarrow$ domestic + Industrial Sewage

Storm sewers $\Rightarrow$ for storm water + ground water
(not for domestic + Industrial)

Combined discharge = Sanitary discharge (domestic + Industrial) + Storm discharge

Sewerage combined system :

• single sewer line of large diameter through which sewage + storm pass to treatment plant

Advantage

① dilution $\rightarrow$ strength $\downarrow$

② self cleansing velocity achieved (✓)

③ economical $\rightarrow$ single sewer line serve double function.

Velocity formula

Manning's formula

$$V = \frac{1}{n} R^{2/3} S^{1/2}$$

Chezy's formula

$$V = C \sqrt{RS}$$

Hazen Williams formula

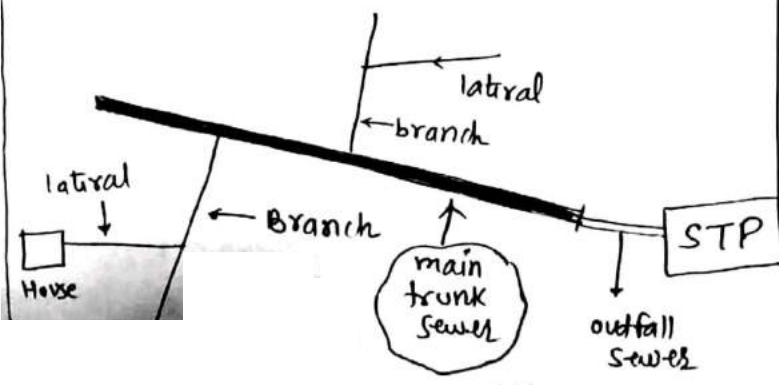
For close conduit / pressure flow

$$V = 0.85 C_H R^{0.63} S^{0.54}$$

Kutter's formula :-

$$C = \frac{\frac{1}{n} + (23 + \frac{0.00155}{S})}{1 + (23 + \frac{0.00155}{S}) \frac{n}{\sqrt{R}}}$$

Design of sewer system :



Self cleansing velocity :-

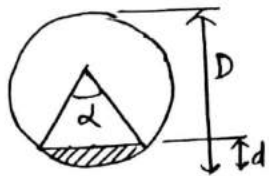
min velocity at which ^{no} solids gets deposited at the bottom of sewer.

Shield's formula :-

$$V = \left[\frac{8\beta}{f} \right] \sqrt{gd(G-1)} \quad \beta = (1-n) \sin \theta$$

↓
Porosity

Hydraulic characteristic of circular sewer :-



Proportional depth	$\frac{d}{D} = \frac{1 - \cos \alpha/2}{2}$
Proportional perimeter	$\frac{p}{P} = \frac{\alpha}{360}$
Proportional area	$\frac{a}{A} = \frac{\alpha}{360} - \frac{\sin \alpha}{2\pi}$
Proportional hydraulic radius	$\frac{r}{R} = \frac{a/A}{p/P}$
Proportional velocity	$\frac{v}{V} = \frac{N}{n} \frac{r^{2/3}}{R^{2/3}}$
Proportional discharge	$\frac{q}{Q} = \left(\frac{\alpha}{360} - \frac{\sin \alpha}{2\pi} \right) \left(1 - \frac{360 \cdot \sin \alpha}{2\pi \cdot \alpha} \right)^{2/3}$

Asper manning's

V_{max}	$\frac{d}{D} = 0.81$	14 % more velocity than full flow
Q_{max}	$\frac{d}{D} = 0.938$	7 % more discharge than full flow

asper chezy's

V_{max}	$\frac{d}{D} = 0.81$	+12.5 %
Q_{max}	$\frac{d}{D} = 0.95$	+5 %

note :-

when 2 sewer's → same degree of self cleansing

$$\therefore r_w r_s = r_w R S$$

$$\textcircled{I} \quad \frac{r}{R} = \frac{S}{s} \quad \textcircled{II} \quad \frac{v}{V} = \frac{N}{n} \left(\frac{r}{R} \right)^{2/3} \left(\frac{s}{S} \right)^{1/2}$$

$$\textcircled{III} \quad \frac{q}{Q} = \left(\frac{a}{A} \right) \cdot \left(\frac{v}{V} \right) \quad \text{put } r/R = S/s \quad \therefore \frac{v}{V} = \frac{N}{n} \left(\frac{r}{R} \right)^{7/6}$$

Hydraulically equivalent :-

$$\text{if } \begin{cases} Q_1 = Q_2 \text{ (full flow)} \\ n_1 = n_2 \text{ roughness} \\ S_1 = S_2 \text{ slope} \end{cases}$$

Ex. circular & squ

$$D = 1.1 B$$

• if min velocity condition not satisfied then

dia. of sewer ↑

increases slope ↑

• In sanitary sewer

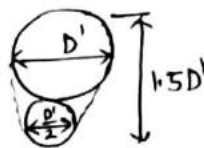
$V_{min} = 0.8 \text{ m/s}$ @ design peak flow
& $V_{min} = 0.6 \text{ m/s}$ @ current peak flow

max. velocity in sewer (concrete) = 2.5-3 m/s

egg shape sewer :-

$$D' = 0.84 D$$

Equivalent section



Circular $\begin{cases} \text{advantage - when } \frac{d}{D} > 0.50 \\ \text{disadvantage - if } \frac{d}{D} < 0.50 \end{cases}$
then velocity reduce

egg shape

→ smaller section ($D'/2$) effective

→ dry weather flow

→ upper large section effective

→ monsoon season.

Time of concentration = overland flow time + channel flow time

note: Before entering manhole, a comb is lowered to check oxygen in manhole.

Peak rate of runoff $q = \frac{1}{36} K_i A \rightarrow \text{ha}$
 $\downarrow \quad \quad \quad \downarrow$
 $\text{m}^3/\text{sec} \quad \quad \text{cm/hr}$

$Q_{eq} = K_1 A_1 + K_2 A_2 / A_1 + A_2$

Design Rainfall intensity = Point rainfall intensity
 or critical rainfall intensity * areal dispersion factor

$P_c = P_o \left(\frac{2}{1 + T_c} \right)$
 $\downarrow \quad \quad \quad \downarrow$
 Point rainfall intensity hr

'or' $P_c = \frac{a}{t + b}$
 $\left(\frac{\text{cm}}{\text{hr}} \right) \quad \downarrow$
 min (time of concentration)

$t < 20$ min	$a = 75$ $b = 10$	$\frac{75}{30}$
$t \geq 20$ min	$a = 100$ $b = 20$	$\frac{100}{40}$

② Junction manhole :- at junction of 2 or more ^{sewer}
 $\rightarrow$ the bottom of small sewer should not be lower than that of larger dia, otherwise reverse flow may happen.

③ Drop manhole :- to connect high level branch sewer to low level by vertical pipe. ($> 0.6\text{m}$)

④ Flushing manhole :- where self cleansing velocity not available then essential to provide some form of flushing device to generate self cleansing velocity.

⑤ Lamp hole :- an electric lamp is inserted into sewer for inspection purpose, if sewer is clear, the light will be visible from adjacent manhole, then cleaning is done accordingly.

⑥ Grease oil trap :- when sewage contain grease & oil, otherwise it will stick to interior surface of sewer then carrying capacity of sewer will be decreased $\downarrow \downarrow \downarrow$.

⑦ Catch Basin :- prevent/eliminate entry of silt, grit from storm water into sewer.

⑧ Storm water Inlet :- to admit surface runoff.

Sewer Appurtenances :

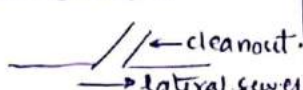
1- manhole : purpose $\rightarrow$ for inspection
 $\rightarrow$ for Testing
 $\rightarrow$ cleaning
 $\rightarrow$ removal of obstruction from sewer line

depth $< 1\text{m}$ normal manhole
 depth $> 1.5\text{m}$ deep manhole

Built at every change of $\rightarrow$ alignment
 $\rightarrow$ gradient (slope)
 $\rightarrow$ diameter
 $\rightarrow$ head of all sewer and branch
 $\rightarrow$ Junction of 2 sewers

dia of sewer (m)	Straight run dist b/w manhole
$0.9 - 1.5$	30 - 150 meter
$1.5 - 2$	150 - 200 meter
$2 - 3$	200 - 250 meter

⑨ cleanout :- provided in lateral sewer in place of manhole.
 ↓
inclined pipe connect from sewer to cleaning of sewer



⑩ :- Inverted siphon :- when sewer pipe has to drop below HGL for passing it beneath a valley.

⑪ :- storm water regulator :- to prevent overloading of sewer pumping station, treatment plant by diverting the excess flow to relief sewers.

Imp.

Generally we design branch sewer only
 $Q_{max} = 3 \times \text{Avg. flow of sewer}$
 $Q_{min} = \frac{1}{3} \times \text{Avg. flow of sewer}$

waste water pipe :- which carry only liquid waste from kitchen, washbasin
note :- It does not carry human excreta.

(note)

Vent pipe

- provide for ventilation Purpose to facilitate the exit of foul gases into atmosphere.

soil pipe

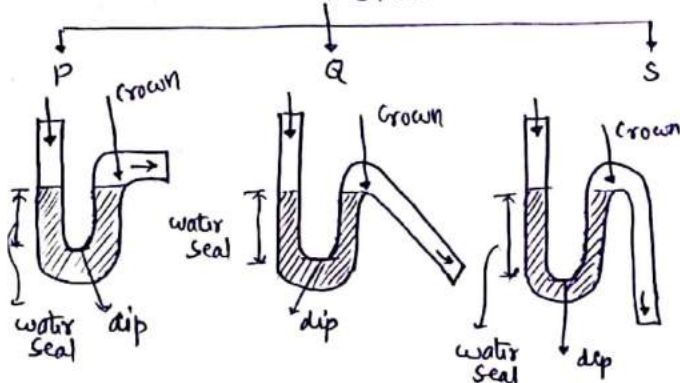
- carry human excreta from water closet to septic tank

Antisiphonage pipe :- ^{separate small dia pipe} installed in house drainage system
 fn → to preserve the water seal of trap.

- helpful to seal the back flow of drainage
- It is connected to Top of 'p' trap **

Trap :- used in household drainage system
 fn → to prevent entry of foul gases in houses

trap types



note :- Intercepting trap :- fn :- disconnect house drain from street sewer

So as to prevent the entry of foul gases of municipal sewer into house drainage system

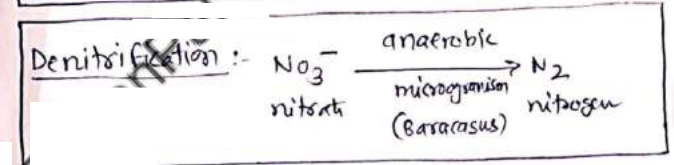
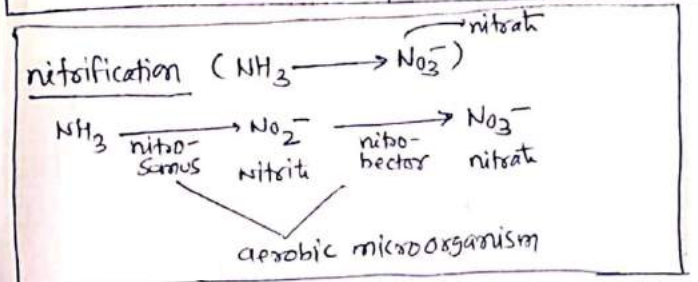
note :- Nahani trap :- Generally used to admit sludge from floor of rooms, bathroom, kitchen.

note :- Gully trap / Gully :- provided at Junction of roof drain and other drain coming from kitchen or bathroom.

note :- 'S' trap / sink trap :- because it is installed under most sinks. of its shape, the trap retains some water after the fixture use.

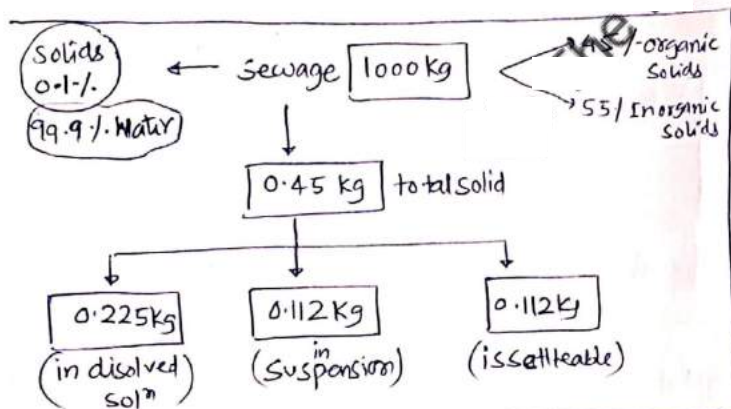
Bacteria/funus	Description
<i>Vibrio cholerae</i>	- gram negative - comma shape bacteria - causes → "cholera" disease - can cause diarrhoea & vomiting in a host within several hours to 2-3 days of indigestion
<i>Entamoeba histolytica</i>	- anaerobic parasitic amoebozoa - infect humans causes amoebiasis
E-coli (<i>Escherichia coli</i>)	- Parasite living only in human or animal intestine - Detection of E-coli in drinking water is taken as evidence of recent pollution with human or animal faeces

Aerobic decomposition (Oxidation happens)	Anaerobic decomposition (Reduction happens)
Carbonaceous $\xrightarrow{\text{ox.}}$ CO_2	Red. $\rightarrow \text{CO}_2$
nitrigenous $\xrightarrow{\text{ox.}}$ NO_3^- nitrate	$\rightarrow \text{NH}_3$
Sulphurous $\rightarrow \text{SO}_4^{2-}$ Sulphate	$\rightarrow \text{H}_2\text{S} \uparrow$
	organic acid $\rightarrow \text{CH}_4 \uparrow$ ↓ methane forming anaerobic bacteria



PH of fresh sewage > 7 (Alkaline)
But as time passes, it becomes acidic because of the bacterial action in anaerobic or nitrification process.

Dissolve oxygen (D.O.) :- min 4 ppm for fish (aquatic)
• determine by → Winkler method
(Oxidation reduction process carried out - chemically to liberate iodine is amount equivalent to the quantity of oxygen originally present.)



Saturation D.O. :- max. quantity of D.O. that can remain mix in water at particulate temp.

Temp.	D.O. (saturated)
0°	14.6 mg/lit
20°c	9.2 mg/lit
30°c	7.6 mg/lit

note :-
oxygen deficit
= $(\text{D.O.})_{\text{saturated at mix temp.}}$

Temp $\uparrow \Rightarrow \text{D.O.} \downarrow$
Chloride content $\uparrow \Rightarrow \text{D.O.} \downarrow$
Pressure $\uparrow \Rightarrow \text{D.O.} \uparrow$
 $\text{D.O.} \uparrow \Rightarrow \text{Corrosion} \uparrow$

—
 $(\text{D.O.})_{\text{actual in stream}}$

- Solids in sewage (0.1%) : [water = 99.9%]
- (i) suspended solid → which remain floating in sewage
 - (ii) dissolve solid → which remain dissolve in sewage (just as salt in water)
 - (iii) colloidal solid → finely divided solids remaining either in solution or in suspension
 - (iv) settleable solid → portion of solid matter, which settles out
↳ measure by Imhoff cone
- 1H. { sewage is allowed to remain undisturb for a period of 2hr in Imhoff cone }

for chemical oxygen demand
Chemical oxygen demand (COD) :-

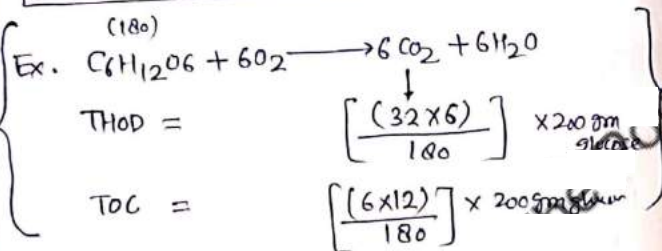
- to measure Biodegradable + nonbiodegradable OM.
- Indicator $\rightarrow$ (ferroin) Test $\rightarrow$ (dichromate test)
- $K_2Cr_2O_7 + H_2SO_4 \xrightarrow{\text{add}} O_2 \text{ measure.}$
Strong oxidising agent

• For most cases $COD \approx ThOD$

Theoretical oxygen demand (ThOD) :-

- by stoichiometry if chemical formula and concentration of OM is known then theoretically calculating oxygen required to completely oxidize the organic matter using balanced chemical reaction.

TOC (total organic carbon) :- to express OM in terms of carbon content.



Imp.

note:- $ThOD > COD > BOD_u > BOD_5 > TOC$

Bio-chemical oxygen demand (BOD) :-

- used as a measure of quantity of oxygen required for oxidation of biodegradable organic matter in water sample by aerobic chemical action.

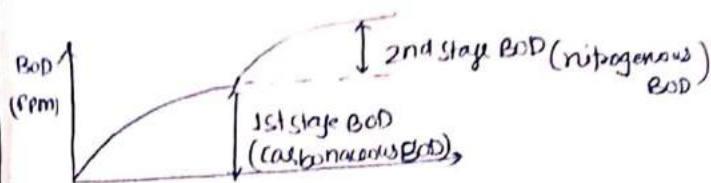
$$BOD_5 = (DO_i - DO_f) \times \text{Dilution factor (DF)}$$

$$\left\{ \frac{\text{volume of diluted sample}}{\text{sewage sample volume}} \right\}$$

if 4% dilution

then $DF = \frac{100}{4} = 25$

$$DO_i = \frac{4 \times DO_{\text{waste}} + 96 \times DO_{\text{aerated water}}}{100}$$



BOD Test :- light excluded $\rightarrow$ to prevent algae growth otherwise they will produce oxygen.

Imp. special case :- when seeded water mix.

20ml $\rightarrow$ waste sample 280ml $\rightarrow$ seeded water

Let initial DO of waste x Seeded water y
Final DO x' " y'

% Initial DO of diluted sample = $\frac{x \times 20 + y \times 280}{20 + 280}$
(waste + seeded water)

Final $\frac{x' \times 20 + y' \times 280}{20 + 280}$

(DO_i - DO_f) diluted = $\frac{(x - x') \times 20 + (y - y') \times 280}{300}$

$BOD_5 = (DO_i - DO_f) \text{ diluted} \times \left(\frac{300}{20} \right) \rightarrow \text{dilution factor}$
 $= (y - y') \times \frac{280}{20}$

Population equivalent :- aim :- used to compare the pollution potential of domestic sewage generated in town & industry.

$$P.E = \frac{\text{Standard } BOD_5 \text{ of Industrial sewage}}{\text{Standard } BOD_5 \text{ of domestic sewage per person per day}}$$

if nothing given $\rightarrow (0.08 \text{ kg/capita/day}) @ 20^\circ C$

Relative stability (S) :- aim $\rightarrow$ to check Test for treatment process

$$S = \frac{O_2 \text{ available in effluent}}{\text{total } O_2 \text{ required for 1st stage BOD (BOD}_u)}$$

$$S = 100 (1 - (0.794)^{t_{20}})$$

$t_{20/37} \rightarrow$ time in days

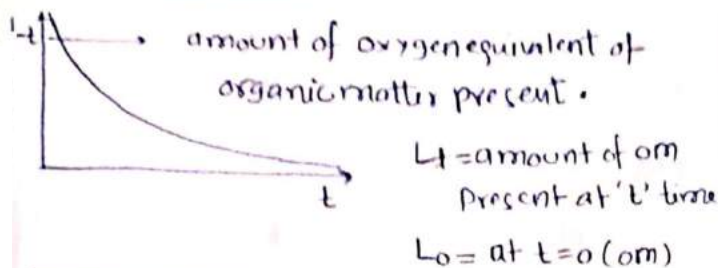
$$S = 100 (1 - (0.630)^{t_{37}})$$

for sewage sample to determine sample of methylene blue

Blue solution when incubated at $20^\circ C / 37^\circ C$

Sooner decoloration $\rightarrow$ earlier anaerobic condition which means less O_2 available

Reaction kinetics



$$\frac{dL_t}{dt} = -kL_t$$

$$L_t = L_0 e^{-kt} \rightarrow \text{exponentially decreases.}$$

$$BOD(y_t) = L_0 - L_t = L_0(1 - e^{-kt})$$

$$\text{at } t \rightarrow 0 \quad (BOD)_t = L_0$$

$$\therefore (BOD)_t = (BOD)_\infty [1 - e^{-kt}]$$

↓
not changed with temp.

Imp

$$\text{Base 'e' } k \times 0.434 = \text{Base '10' } k_D$$

tap water	k_D (/day) 0.05
surface water, treated sewage	0.05 - 0.10
municipal sewage	0.10 - 0.15

Habit

k_D range
 ≈ 0.10 /day

Van't Hoff - Arrhenius eqn.

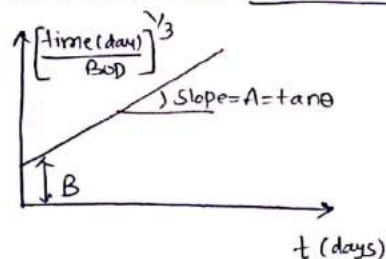
$$k_D (\text{deoxygenation constant}) = k_{D_{20}} (1.047)^{T-20}$$

$$k_{R_T} (\text{reoxygenation constant}) = k_{R_{20}} (1.016)^{T-20}$$

temp. coefficient

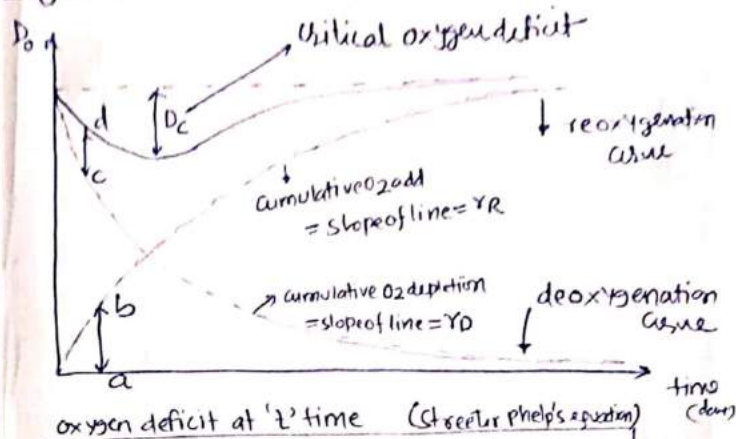
$$k_{R_{20}} = \frac{3.9 \sqrt{V}}{y_{1.5}}$$

k_D experiment (Thomas Graphical solution)



$$k_D = 2.61 \frac{A}{B} \text{ day}^{-1}$$

Sag curve



$$D_t = \frac{k_D \cdot L}{k_R - k_D} \left[10^{-k_D t} - 10^{-k_R t} \right] + D_0 10^{-k_R t}$$

L → ultimate BOD of mix at point of discharge

initial oxygen deficit

$$t_c = \frac{1}{k_D(f-1)} \log \left[\left(1 - (f-1) \frac{D_0}{L} \right) f \right]$$

f → self purification constant

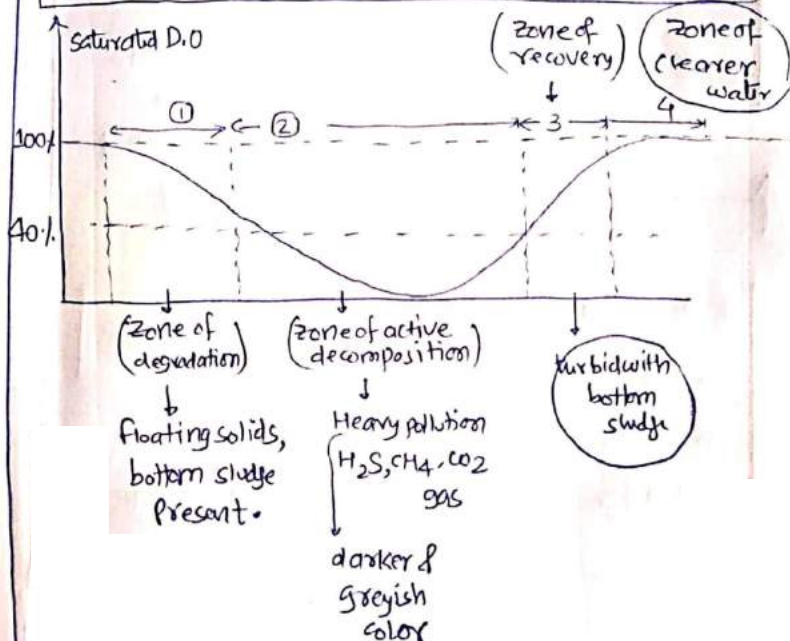
$$\left(\frac{L}{D_c f} \right)^f = \left(1 - (f-1) \frac{D_0}{L} \right) f$$

$$f = \frac{k_R}{k_D} \text{ at mix temp.}$$

Deficit max (D_c) where rate of re-aeration = rate of oxygenation

Mechanism of self purification

- (i) Dilution & dispersion
- (ii) Sedimentation → suspended solid settled.
- (iii) sunlight → photosynthesis, oxidation of OM
- (iv) oxidation of organic matter
- (v) reduction → Hydrolysis of organic matter.



Self purification depends :-

- (i) temp. (ii) turbulence (iii) Amount & type of organic matter
- (iv) Hydrography of river stream
- (v) Rate of regeneration.

Lake pollutant :- major pollutant - **phosphorus**

- (max. killing during mixing)
aquatic animal

lake layers :-

- (i) upper layer → warm layer → **Euplimnion** 
(mixed sufficient O₂)
 - (ii) middle layer → region of temp. gradient
→ **Thermocline / metalimnion**
 - (iii) lower layer → **Hypolimnion** → cool layer
(unmixed) (less O₂)
- late stratification → changes.

Productivity of Lake :-

- ability to support food chain
- 'or' measure of Algae growth

order of productivity :-

oligotrophic < mesotrophic < eutrophic < **senescent lake**

↓
very old lake
which almost
becomes
marshy.

$$\text{Dilution factor} = \frac{Q_s + Q_r}{Q_s}$$

Dilution Factor	treatment needed / given
> 500	no treatment given, directly discharge
300 - 500	plain sedimentation (Primary sedimentation)
150 - 300	sedimentation + screening + chemically ppt
< 150	complete treatment

Biological zones in lake :-

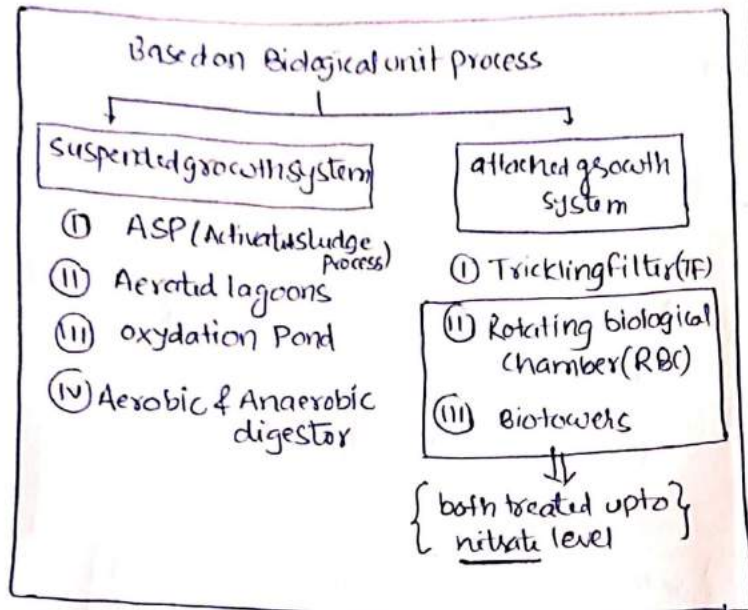
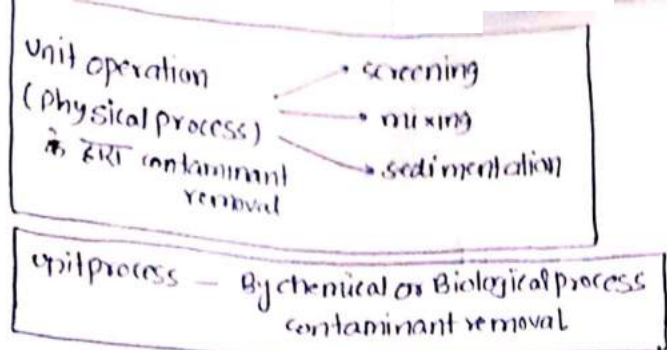
(i) Euphotic zone	till where sunlight penetrates if turbidity ↑ EZ ↓
(ii) Littoral zone	where rooted plant grow
(iii) Benthic zone	• Bottom sediments in lake which contain Bacteria • living organism → settled hence decompose by bacteria.

Eutrophication in lake :-

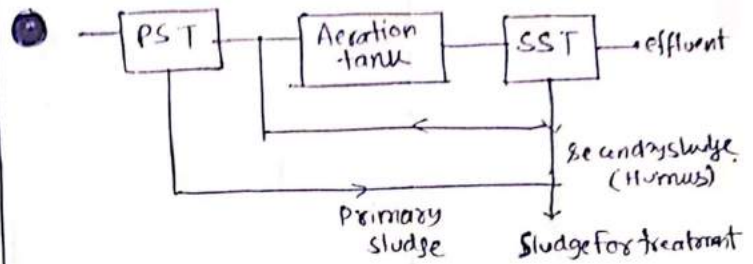
due to Excessive N, C, P

- Lake + excessive Algae

How to avoid → lakes should not be used for disposal of even treated sewage

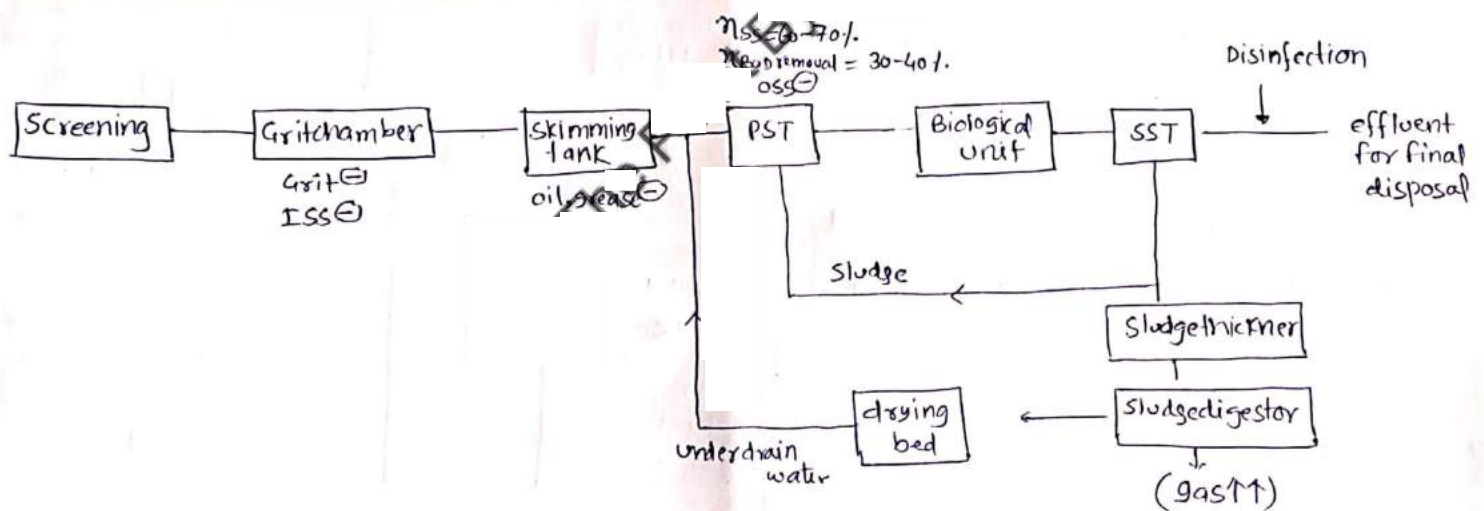


- (2) Primary treatment → Primary treatment + PST (remove suspended solids)
- (3) Secondary treatment: (remove colloidal & soluble organic matter)
- [Biological conversion of dissolved & colloidal OM into Biomass]



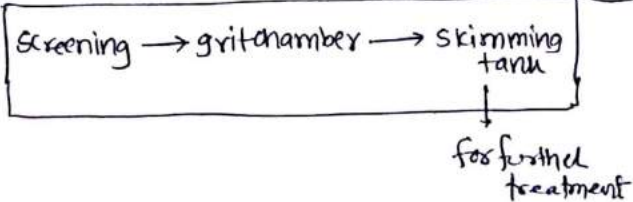
- (4) Tertiary Treatment: to meet effluent standard

(river → if used as source of water supply then tertiary treatment is must before disposing treated waste into it.)



(1) Preliminary treatment system:

fn → remove (floating material) + large inorganic particulate content



note:- Before skimming tank → parshall flume or other velocity control device

unit	detention time (td)	unit	time
Grit chamber	40 - 60 sec.	Sludge digestion	30 days
Skimming tank	3 - 5 min.		
vacuator	10 - 15 min		
SST	1.5 - 2 hr.		
Imhoff tank	2 hr		
PST	2 - 2.5 hr.		
septic tank	24 hr.		
oxidation pond	15 - 30 days		

Sludge process	Description	
Sludge thickening	water removal (for reduction of sludge volume) basically	(i) Gravity thickening → for primary sludge + ASP sludge (not for ASP sludge alone) (ii) Air Floating → normally used for ASP sludge (iii) centrifugation → where space restriction
Sludge conditioning (increase drainability of sludge)	water removal (sludge volume ↓↓)	(i) heat treatment (ii) chemical treatment
Sludge stabilization	digestion	• generally by Anaerobic process
Reduction of Sludge	volume decreases by chemical oxidation	

① Screening :- remove certain piece of wood, debris
→ protect pump & other mechanical equipment

② communion & maceration :-
↓ Cutting ↓ Grinding.

③ Grit chamber :- remove Grit, sand (> 24)
(Inorganic suspended solid)
↓
advantage :- reduce frequency of cleaning of sedimentation tank, digester

$$V_h = 0.15 - 0.30 \text{ m/s}$$

$$t_d = 40 - 60 \text{ sec.}$$

$$V_c = K_c \sqrt{g d (G - 1)}$$

(horiz) (vert) (3-4)

length of channel increase by 20% as an allowance.

note:- velocity control device

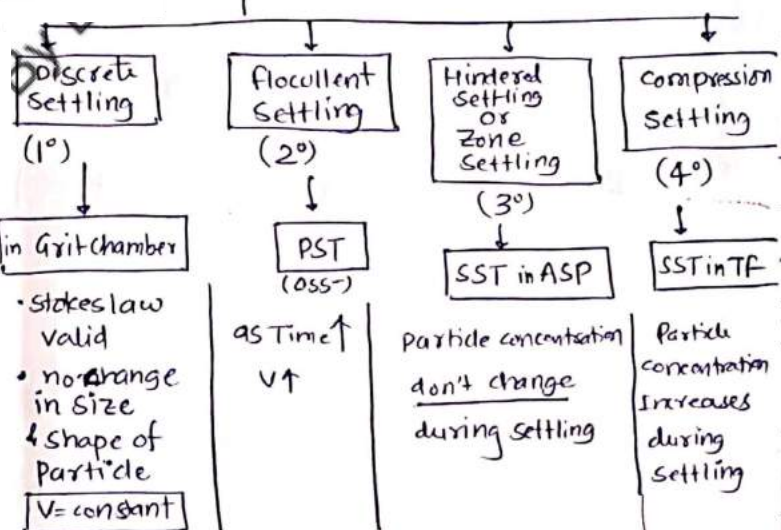
for Rectangular section
Proportional weir provided

for Parabolic section
Parshall Flume provided

④ Detritus tank :- same as grit chamber only difference it removes finer inorganic ss.

⑤ Removal of oil, grease, soap
↑ Skimming tank $t_d = 3 \text{ to } 5 \text{ min}$
↓ Vacuumator $t_d = 10 - 15 \text{ min}$
before sedimentation tank provided.

⑥ Sedimentation → organic suspended solid settled (under gravity)



Secondary treatment (Biological Treatment)

Aerobic treatment

- (i) Trickling filter
- (ii) ASP
- (iii) Aerated lagoon
- (iv) oxidation pond

Anaerobic Treatment

- (i) septic tank
- (ii) Imhoff tank
- (iii) Upflow Anaerobic Sludge blanket (UASB)
↓
Used for Industrial Sewage

Attached growth system

- TF
- RBC
- Biower
- Biomass attached to medium & sewage containing OM is passed through medium

Suspended growth system

- Biomass is in suspension in liquid containing OM

Trickling filter (attached growth system)

- Predominant organism → Facultative bacteria
- each TF must be having SST (due to removal of Biomass) 'or' sloughing

TF

Standard Rate TF

$$R = 0 \quad F = 1 \quad (\text{no recirculation})$$

High rate TF

$$R > 0 \quad F > 1 \quad R = 1 \text{ f} = 1.65 \quad R = 1.5 \text{ f} = 1.89$$

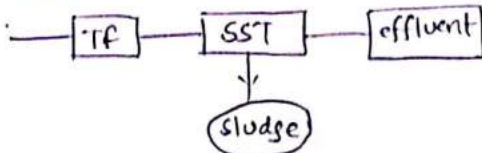
F → recirculation factor

$$F = \frac{1 + R}{(1 + 0.1R)^2}$$

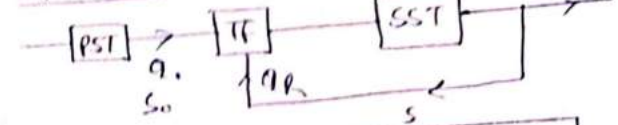
Recirculation ratio $\frac{Q_R}{R = Q_0}$

$0.1 = 1 - f$ → treatability factor which is 0.9 for sewage

conventional (Standard Rate TF) ∴ (no recirculation)



High rate TF:



$$R = \frac{Q_R}{Q_0}$$

$$\eta = \frac{100}{1 + 0.0044 \left[\frac{Y}{VF} \right]}$$

Applied load to TF (kg/day)

note: Organic loading rate = $\frac{Y}{V}$ (kg/ham/day)

note: TF design → Avg. flow
distributory arm → Peak flow under drainage pipeline (check for Avg. flow)

Rate of food removal depends (TF)

Hydraulic loading rate (HLR) or HOC rate (m³/m²/day)

(HLR ↑ Sloughing ↑)
↓
net removal of Biomass film

organic loading rate OLR (kg/ham/day)

OLR ↑
• rapid growth of Biomass
∴ plugging of pores & flooding of tank

temp

Rate of diffusibility of food & O₂ into Biofilm

operational trouble in Standard Rate TF (R=0)

filter media Ponding & Clogging

when OLR ↑

Solution: ∴
• wash filter
• add CuSO₄ to prevent growth of Algae
• chlorinated sewage

Excessive fly breeding

solⁿ: reduced by flooding for 24 hrs.

solⁿ: do chlorinating

odour

due to H₂S ↑

• Cl₂ being oxidising agent oxidise H₂S

High Rate Trickling Filter :- Design :-

① Surface area of TF = $\frac{Q_0 + Q_R}{HLR} \frac{m^3/d}{m^3/m^2/d}$
(include recirculation)

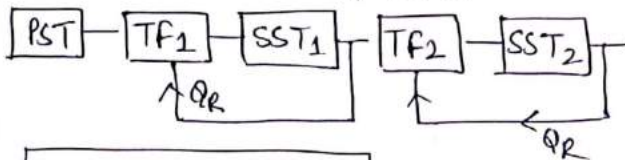
② Volume of TF = $\frac{Q_0 S_0}{OLR} \frac{kg/d}{kg/hm^2/d}$
(exclude recirculation) (excluding recirculation)

RBC (Rotating Biological chamber)

→ treatment upto nitrate level

- take advantage of both $\left\{ \begin{array}{l} \text{suspended growth system} \\ \text{attached growth system} \end{array} \right.$

Two stage TF :- (adopted if BOD_{in} → more
if BOD_{out} → less we want.)



$$\eta_1 = \frac{100}{1 + 0.0044 \sqrt{\frac{Y_1}{V F_1}}}$$

$Y_2 = Y_1 (1 - \eta_1)$ → BOD removal efficiency

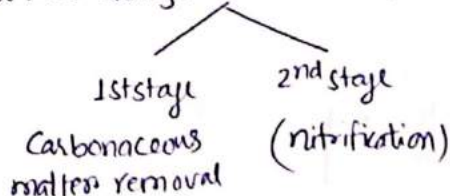
$$\eta_2 = \frac{100}{1 + \frac{0.0044}{(1 - \eta_1)} \sqrt{\frac{Y_2}{V F_2}}}$$

Advantage of High Rate TF :-

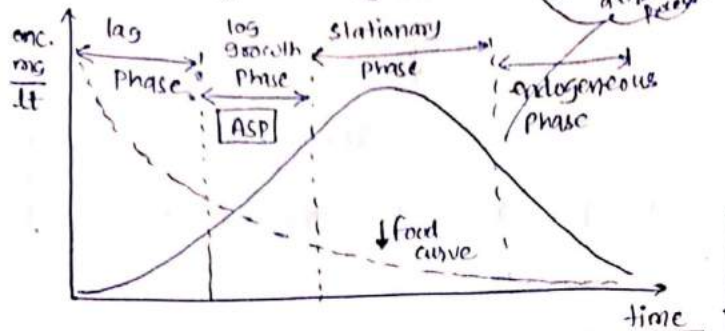
- BOD removal $\eta \uparrow$ But nitrogenous matter

may not get sufficient time for nitrification as rate of flow is fast, Biological film may get sloughed before nitrification has had time to take place.

So to avoid this 2 stage filtration →



Activated sludge process (ASP): (Suspended growth system)

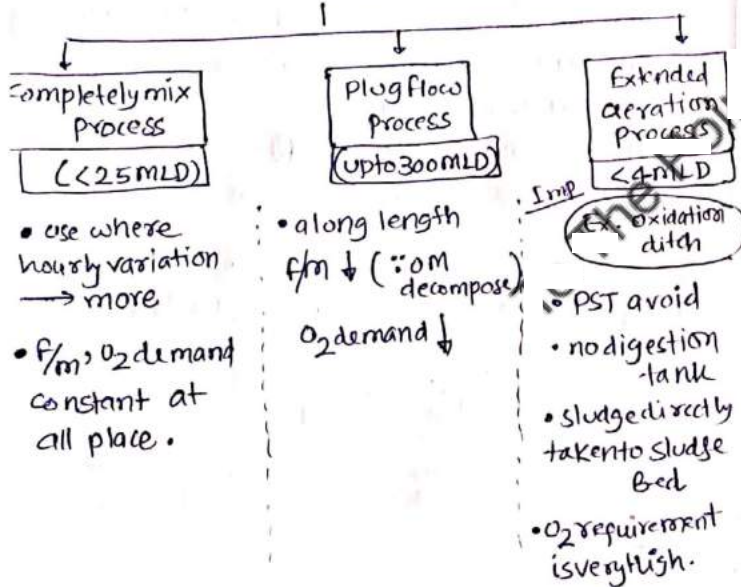


MLSS $\Rightarrow$ Inorganic + dead $\Rightarrow$ living + dead bacteria
MLVSS $\Rightarrow$ 80% of MLSS (only organic)

ASP $\rightarrow$ in this settled sludge in SST [containing living organism]

returned to aeration tank (reactor) to increase the available biomass (rich in microbial mass) & speed up the reaction.

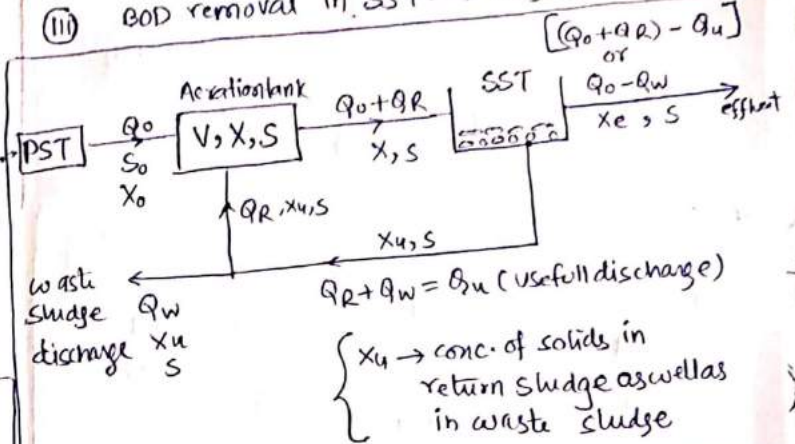
Process



Complete mix process :-

Assumption (i) Influent, effluent biomass concentration (X_0) (X_e) negligible as compare to biomass at other point.

- (ii) all reaction occurs in reactor (aeration tank)
- (iii) BOD removal in SST $\rightarrow$ negligible ($S \rightarrow S$)



Design parameters :-

(i) Aeration time detention time Hydraulic retention time $= \frac{V}{Q_0}$ (volume of tank) (rate of flow in tank) excluded recirculation

(ii) Organic loading rate (OLR) volumetric $= \frac{Q_0 S_0}{V}$ kg/hmld. (mass of BOD Applied / Volume of A-Tank)

(iii) Specific substrate utilization $U = \frac{Q_0 (S_0 - S)}{VX}$ (mass of BOD remove in tank / mass of Biomass in tank)

(iv) Food Applied Biomass $f/m = \frac{Q_0 S_0}{VX}$ { when $S \rightarrow 0$ then $S_0 \gg S$ }

$f/m \uparrow \Rightarrow BOD \text{ removal } \downarrow (\eta \downarrow)$
 $\eta \downarrow \Rightarrow Q_W \uparrow$ (Temp $\uparrow \Rightarrow Q_W \uparrow$)

note:-

$$\frac{1}{\theta_c} = \frac{Yg - K}{\frac{Q_0 S_0}{VX}}$$

sludge age

- ⑥ Sludge age (θ_c) → avg. time for which biomass remain in system.
 ↳ indicate residence time of Biological solid in system.

$$\theta_c = \frac{Vx}{(Q_0 - Q_w)x_e + Q_w x_u}$$

→ mass of MLSS in tank
 → mass of MLSS leaving system per day.

if $x_e \rightarrow$ neglect
 $\left\{ \theta_c = \frac{Vx}{Q_w x_u} \right\}$ ($Q_w \downarrow \theta_c \uparrow$)

- ⑦ Sludge volume Index (SVI) range → 50-150 $\frac{\text{mL}}{\text{gram}}$

- ① SVI → volume occupied by 1 gram of solid in mixed liquor after settling for 30 min.

$$SVI = \frac{V_{0.6}}{x_{0.6}} \times 1000 \quad \frac{\text{mL}}{\text{gram}}$$

$$SVI = \frac{10^6}{x_u}$$

→ Settled volume in 1000 mL $\frac{\text{mL}}{\text{gram}}$
 → concentration of SS in mixed liquor (mg/L)

- ② SVI → decides rate of recycle of sludge (Q_R)
 req. to maintain desired MLSS (x),
 F/M in tank to achieve required degree of purification.

- ③ Sludge recirculation & settleability determined by SVI.

⑦ Sludge density Index (SDI) = $\frac{100}{SVI (\text{mL/gram})}$

⑧ Recirculation ratio $\Rightarrow R = \frac{Q_R}{Q_0} = \frac{x}{x_u - x}$

not: mass balance eqn in AT

$$Q_0 x_0 + Q_R x_u = (Q_0 + Q_R) x$$

$$SVI = \frac{10^6}{x_u}$$

Imp point in ASP :-

- ① most imp. aspect to maintain F/M ratio which is done by $\begin{cases} \text{MLSS} \uparrow \\ \text{MLSS} \downarrow \end{cases}$ depend on influent BOD load.
- ② $Q_w \uparrow$ F/M $\uparrow$ Temp $\downarrow$ BOD removal $\downarrow$

Sludge Bulking :- → (poor settling characteristic)

- due to inadequate air supply resulting in lower F/M septicity → leads to filamentous organism.

- filamentous organism → form due to low nutrient concentration

• growth of filamentous organism

- supported by $\begin{cases} \theta_c \uparrow (\text{High sludge age}) \\ F/M \downarrow (< 0.3) \\ T \uparrow \end{cases}$

note: Sludge Bulking control :-

- ① $\theta_c \downarrow (< 6 \text{ day})$
- ② chlorination of returned activated sludge
- ③ addition of nutrient if less
- ④ add lime or soda
- ⑤ Increase recycle ratio (R)
- ⑥ Increase rate of aeration.

Imp note:

rise of sludge → caused by denitrification

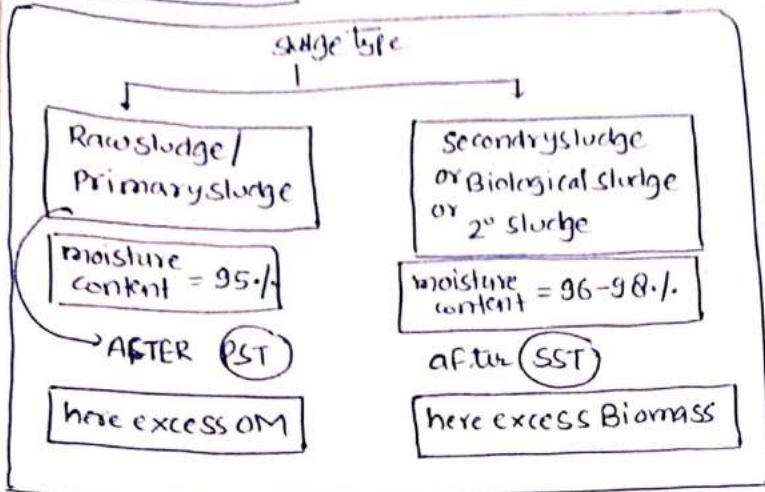
conventional nitrification → by Autotrophic

Biological nitrogen removal → by Nitrifiers & denitrifiers.

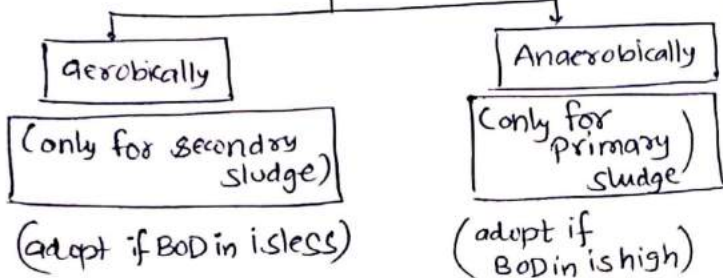
Imp note:

process	% of BOD removal
oxidation ditch (extended aeration)	98 %
oxydation pond	90 % (symptomatic reblow)
TF	80-90 %
ASP	80-95 %

Sludge digestion :



Sludge digestion

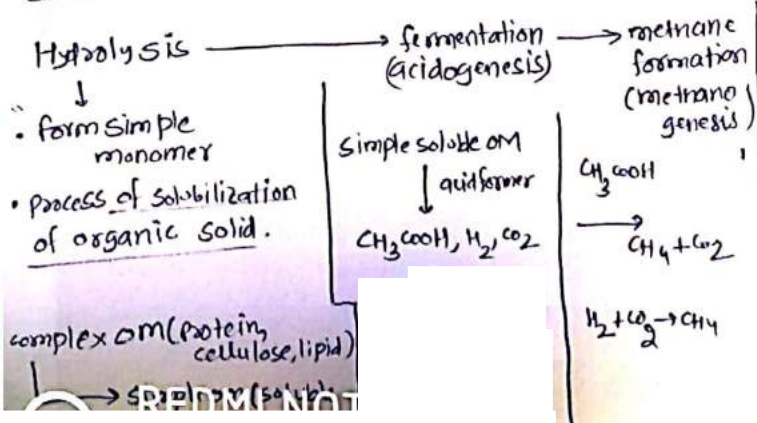


- Extension of extended aeration process.
(there is scarcity of here food, endogenous respiration will start)
- digested sludge consist of cell walls, cell fragments
- energy consumption → more
- This sludge dewater poorly.

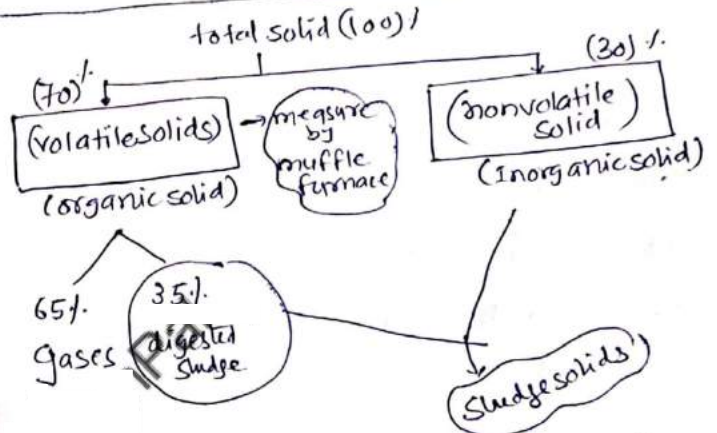
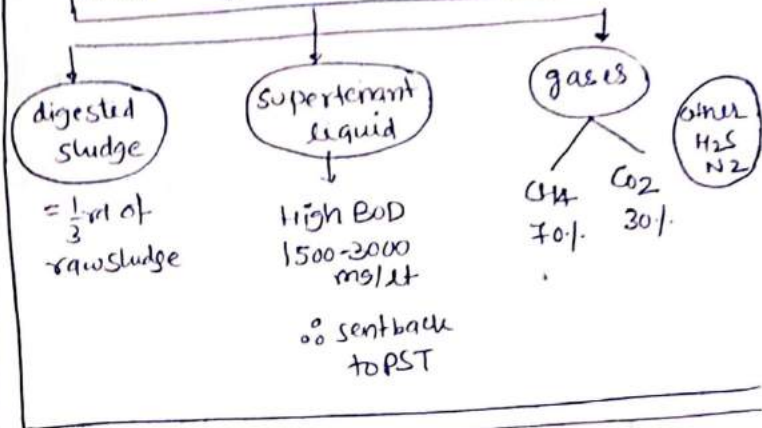
Gases released
CH₄ CO₂

stages in sludge digestion :-

Acid fermentation — acid regression — Alkali fermentation — methane formers

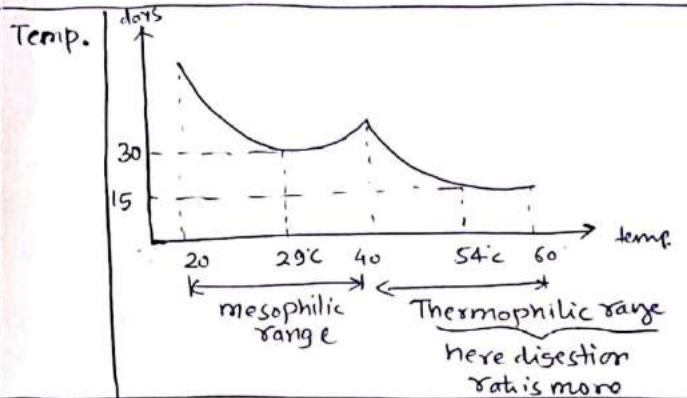


Anaerobically sludge digestion process



Gas produced = $0.6 \text{ m}^3/\text{kg}$ volatile solid present
methane heat content = 8600 Kcal/m^3

factor's affecting sludge digestion



PH
pH ↑ rate ↑
• if pH of sludge drops down to low value Bacterial action will get suppressed resulting in reduced digestion rate.

Seeding with digested sludge

mix & steering of raw sludge

Nuisance organism

V.Smp

$$V_1 (100 - P_1) = V_2 (100 - P_2)$$

Volume Moisture content.

digestor Capacity

Parabolic variation

Straight line variation

undigested → digested

$$V = \left(\frac{V_1 + 2V_2}{3} \right) t + V_2 T \quad \text{or} \quad \left[V_1 - \frac{2}{3}(V_1 - V_2) \right] t + V_2 T$$

$$V = \left(\frac{V_1 + V_2}{2} \right) t + V_2 T$$

monsoon storage

digestion period (30 days)

SST (Secondary Sedimentation tank) :-

- ① must produce an effluent sufficient clarified.
- ② They must concentrate the biological solids to minimize the sludge to be handled.

③ design basis

loading Solid rate
 $area = \frac{Q_0 + Q_R}{\text{Solid loading rate}}$

Hydraulic loading rate
 $area = \frac{Q_0}{\text{overflow rate}}$

④ detention time $\Rightarrow 1.5 \frac{hr}{2}$
 (otherwise denitrification will occur & N₂ will evolve)

note:- All units of treatment are kept above HFL of river except sludge drying bed hence during flooding, only sludge drying bed is flooded, rest is operational.

Oxidation Pond :-

$$t_d = \frac{1}{K_D} \log \frac{L_{in}}{L_{out}}$$

- open flow earthen Basin
- long detention period (15-30 days) during which waste get stabilized by action of natural force.
- algae symbiosis occurs (oxygen demand is met by combined action of Algae & other micro-organism)

Depth - (1-1.5m)

t_d - 15-30 days

$L/B = 3$ $L > 750$ m

each unit = 0.5-1 ha

Pathogenic bacterial removal = 99.9%

BOD removal = 90% (80-90%)

Septic tank :- ordinary settling tank with large detention time (24-36 hr) with extra provision for sludge digestion by anaerobic bacteria.

- Flow of sewage = 40-70 lpcd
- detention time = 24-36 hr
- Rate of accumulation = 30 lpc per year of sludge
- cleaning period = 6-12 month (0.5-1 yr)
- min width = 0.75m (min liquid capacity = 1000 litres)
- $L/B = 3$
- free board = 0.30

Imhoff tank :- use in case of small treatment plants require only primary treatment

upper lower portion (chamber)
sedimentation digestion

oxidation ditch :- (extended aeration system)

- no PST
- no digester
- In this Biological solids produced are destroyed by endogeneous respiration and separate sludge handling not required.

Solid waste management :

① Composting method

- Biological method of decomposing solid waste
- used when → high organic content & high moisture content
- final product → manure*

Process



∴ (turn mass either manually or mechanically)

• turning not required ∴ more clean than Indore method

② Sanitary land filling method

- used when → high density
- layer of 300-600mm
- Leachate formed
- non biodegradable + acid + water matter
→ carcinogenic compound.

③ Autoclaving

- low heat treatment process for biomedical waste under controll. temp.

④ Incineration

- adopt when → MSW has high calorific value.
- Burn of refuse in presence of O_2 (oxygen)

⑤ pulverization

refuse pulverised by grinding machine

⑥ pyrolysis

- limited / nil presence of O_2
- for plastic & rubber

⑦ deep well Injection method

- for disposal of liquid hazardous waste
- expensive
- It poses a danger of leakage hazardous waste and eventually polluting subsurface water supplies

18/3/20

Primary air pollutants :- directly emit from identified source.

- ① Particulate matter
- ② Sulphur compounds (SO_2)
- ③ oxide of nitrogen (NO_x) $\begin{matrix} \nearrow \text{NO} \\ \searrow \text{NO}_2 \end{matrix}$
- ④ Carbon monoxide (CO)
- ⑤ Halogen compounds (methyl & ethyl mercaptans)
- ⑥ Volatile organic matter (hydrocarbon)
- ⑦ Radioactive compounds

others $\text{CH}_4 / \text{NH}_3 / \text{CFC} / \text{toxic metals}$.

Secondary pollutant :- produced in air by interaction among two or more primary pollutants, or by reaction with normal atmospheric constituent with or without photoactivation.

- ① $\text{H}_2\text{SO}_4 \longrightarrow \text{SO}_2 + \text{O}_2 (\text{DO})$, when water drops are present in atm.
- ② Ozone (ground level)
- ③ Formaldehyde (HCHO)
- ④ PAN (peroxy acetyl nitrate)
- ⑤ Photochemical smog

NAQI (National Air Quality Index)

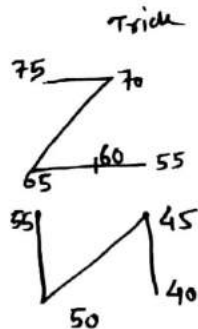
8 pollutants $\Rightarrow \text{PM}_{10} / \text{PM}_{2.5} / \text{NO}_2 / \text{O}_3 / \text{CO} / \text{SO}_2 / \text{NH}_3 / \text{Pb}$

6 category

- Good (0-50)
- Satisfactory (51-100)
- Moderately (101-200)
- Poor (201-300)
- Very poor (301-400)
- Severe (401-500)

V.V.S.M.B Ambient Air quality standard Leq (dB)

Zone	day	night
Industrial	75	70
Commercial	65	55
Residential	55	45
Silence	50	40



Sound pressure level $L_p (\text{dB}) = 20 \log \left(\frac{P_{\text{rms}}}{20 \mu\text{Pa}} \right)$

note: Man $\begin{cases} \text{min } 20 \mu\text{Pa} & 20 \text{ Hz} \\ \text{max } 200 \text{ Pa} & 20000 \text{ Hz} \end{cases}$

Sound Intensity level $\text{dB} = 10 \log \left(\frac{I}{I_0} \right)$

$\because I \propto P_{\text{rms}}^2$

10^{-12} W/m^2

Sound power level $= 10 \log \frac{W}{(10^{-12})}$ $\rightarrow \frac{W}{\text{m}^2}$

Note

$L_p + L_p \xrightarrow{\text{Pressure}} \sqrt{2} L_p \quad \{ \sqrt{I_1^2 + I_2^2} \}$

$I + I \xrightarrow{\text{Intensity}} 2I$

$P + P \xrightarrow{\text{Sound power}} 2P$

Sound power (watt) $= 4\pi R^2 \times I$

net $P_{\text{rms}} = \sqrt{P_{\text{rms}}^2 + P_{\text{rms}}^2}$

Difference in noise level	Increase in noise Pollution (बढ़े जाने से)
0-1	3
2-5	2
6-8	1

Ex. $70 \text{ dB}, 70 \text{ dB} \longrightarrow 70 + 3 = 73 \text{ dB}$
 $70, 73 \text{ dB} \longrightarrow 73 + 2 = 75 \text{ dB}$

Average sound :-

$$L_{\text{avg}} = 20 \log \left(\frac{10^{L_1/20} + 10^{L_2/20} + \dots}{N} \right)$$

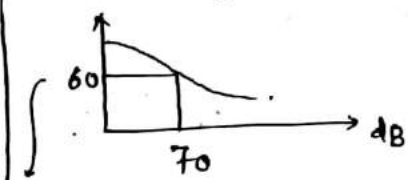
equivalent sound :-

$$L_{\text{eq}} = 10 \log \left[10^{L_i/10} \times \text{fraction of time} \right]$$

noise rating system $\begin{cases} L_n \\ L_{eq} \end{cases}$

① L_n concept (statistical concept) :-

Sound pressure level that will exceed for N.% of gauging time.



Ex. 70 dB of L_{60}

Sound level will exceed 70 dB for 60% of measuring time

% of time $\geq$ standard value

② L_{eq} concept :- constant noise level which over a given time expands the same amount of energy as is expanded by the fluctuating level over the same time.

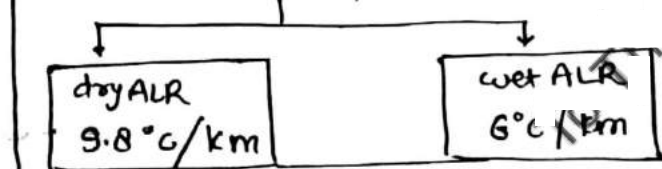
Ex. $L_{eq}(8)$ $\rightarrow$ 8 hr. measurement
if nothing is given $\rightarrow$ then it is for 1 hr.

Lapse rate :- In troposphere ,
temp of ambient air $\downarrow \Rightarrow$ if Altitude $\uparrow$
(height)
this rate of change of temp. is called
lapse rate.

Environmental lapse rate (ELR) :- $\{T_H\}$
or Ambient lapse rate or
Prevailing lapse rate

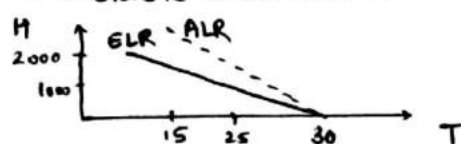
• send balloon (equipped with thermometer)
 $\rightarrow$ self recording mechanism

Adiabatic lapse rate (ALR) :-
when parcel of air (which is hotter and
higher than surrounding air) is released,
then naturally it tends to rise up untill
a level at which its own temp. and density
becomes equal to that of surrounding air,
this rate of decrease of temp. with height
 $\rightarrow$ adiabatic lapse rate.



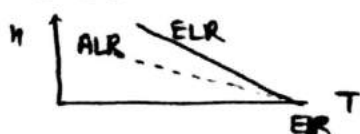
① Superadiabatic lapse rate (ELR > ALR)

$\rightarrow$ unstable environment



② Subadiabatic lapse rate (ELR < ALR)

$\rightarrow$ Stable environment



③ Neutral lapse rate (ELR = ALR)

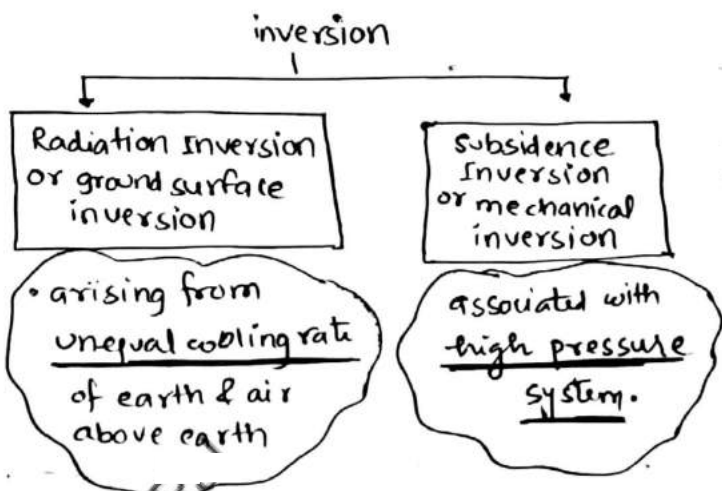
Negative lapse rate / Inversion :-

temp $\uparrow$ if H $\uparrow$

$\frac{\partial T}{\partial H}$

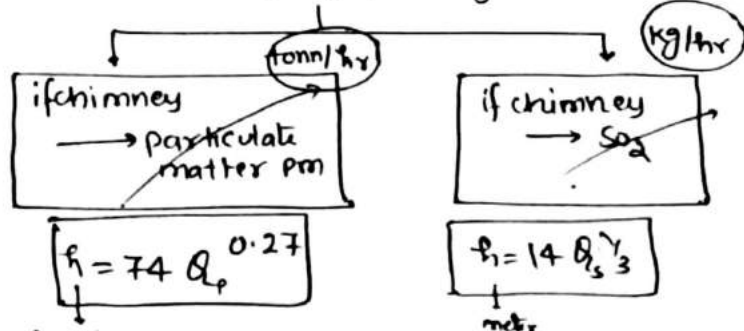
मलब - state in which warm air lies below cold air

• inversion may be near earth surface
and greater height.



double inversion = Radiation Inversion + Subsidence Inversion

Design of stack height



But

min stack height

Industry $\Rightarrow$ 30 meter

Thermal power plant

200-500 MW

220 meter

> 500 MW

275 meter

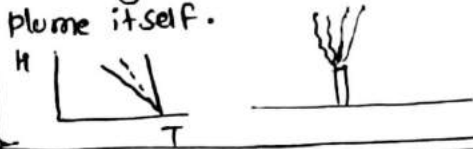
Plume :- path taken by continuous discharge of gaseous effluent emitted from stack / chimney.

- The shape of path and concentration distribution of gaseous plumes depends upon localised air stability.

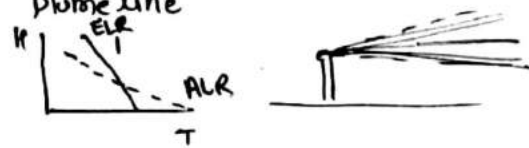
- ① Looping plume :-
- most common type plume under superadiabatic lapse rate ($ELR > ALR$)
 - condition $\rightarrow$ light to moderate wind speed on a hot summer afternoon when large scale thermal eddies are present
 - High turbulence $\rightarrow$ rapid dispersion of plume but high concentration touch the ground.



- ② Neutral plume :- ($ELR = ALR$)
- upward drifting of plume will continue till air density becomes similar to that of the plume itself.



- ③ Coning plume :- in cloudy day / night $v > 32 \text{ kmph}$ ($ELR < ALR$) when lapse rate is near neutral.
- Plume shape is vertically symmetrical about plume line



- ④ Lifting plume :- in strong superadiabatic lapse rate above inversion.

(Best / Ideal plume)

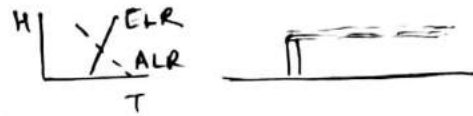
$\because$ downward motion & mixing is

Prevented by surface inversion but upward-mixing will be quite turbulent and rapid.



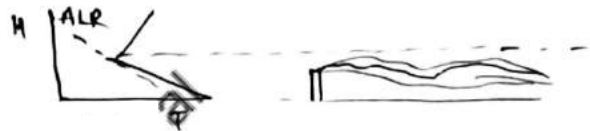
- ⑤ Fanning plume :-

- in extreme inversion condition in the presence of light wind.
- most of the vertical dispersion is suppressed by extremely stable condition, plume fans out in the horizontal direction

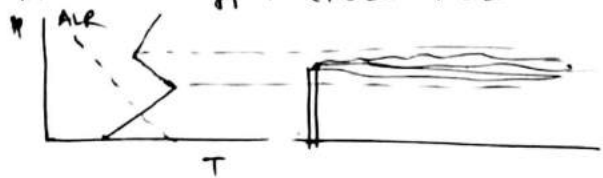


- ⑥ Fumigation plume :- worst plume

- just inversion of lifting plume.
- fumigation takes place when an inversion layer occurs at a short distance above the top of stack and superadiabatic conditions prevail below it.

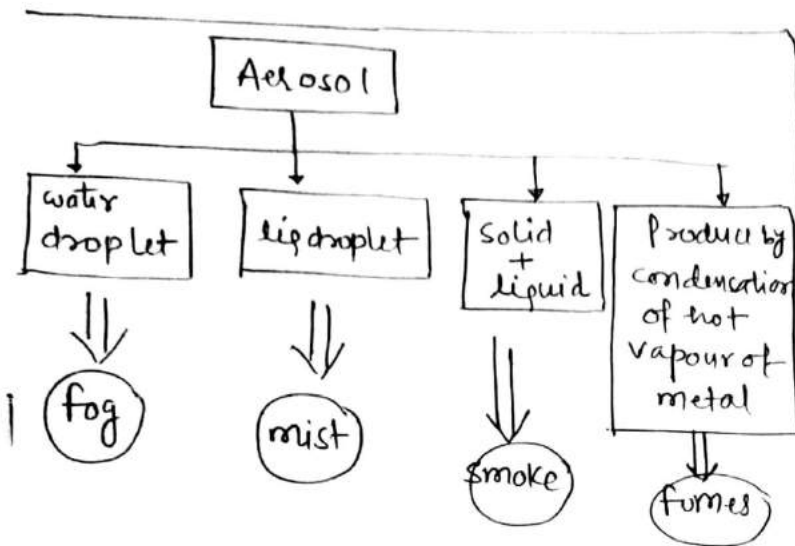


- ⑦ Trapping plume :- when plume caught between 2 inversion layers, hence the emitted plume can neither go up nor down and will be trapped between the 2 levels.



method of removing particulate matter :-

equipment	particle size removed	remarks
Gravitational ① settling chamber	large particles ($> 50 \mu\text{m}$)	• simple design • low efficiency require more space • low pressure loss
cyclone collector ↓ separator ② use of centrifugal force	($40-50 \mu\text{m}$)	• simple to design & maintain • require less floor area • low to moderate pressure loss
③ fabric filter	filter bag usually tubular ($< 1 \mu\text{m}$) $\eta = 99\%$	• high efficiency • The flue gas must be dry to avoid condensation & clogging. The fabric is liable to chemical attack.
④ electrostatic Precipitator $\eta = 1 - e^{-\frac{WA}{Q}}$ A → collector Plate area (m^2)	$\approx 1 \mu\text{m}$ $\eta = 95-99\%$ • very small particles also wet & dry can be easily trapped. • more than 99% efficiency can be achieved in their functioning	• mostly used in Industry - thermal Power Plant - cement plant - Paper mill • gas is flown in high voltage field
⑤ wet scrubber venturi scrubbers	sub • can remove gaseous as well as particulate contaminant ($0.5-5 \mu\text{m}$)	• suit for removal of submicron particulate associated with smoke & fumes.
spray tower	low cost handling of large volume of gases	
wet cyclone scrubbers	higher efficiency than spray towers.	



Nox

- automobile exhaust
- effluent in Industry where HNO_3 (nitric acid) present

CO
(asphyxiant)

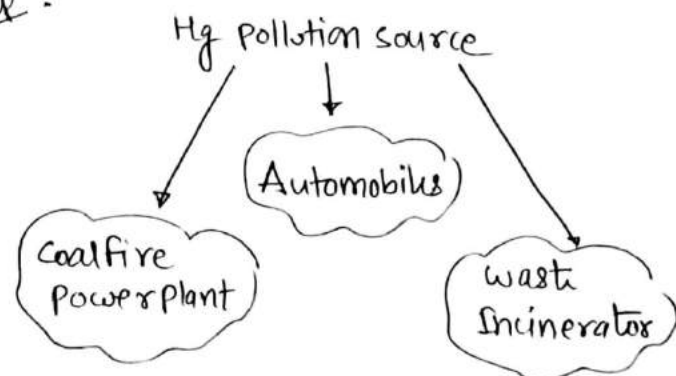
- due to Incomplete combustion of Carbonaceous material (especially due to automobile exhaust)

Aldehyde

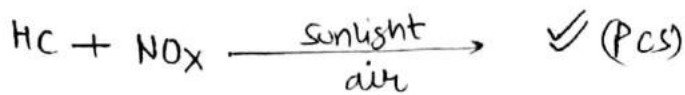
- formed by combustion of gasoline, diesel oil, fuel oil, natural gas.
- formed in air due to photo-chemical reaction.

Gas	Source & remark
H_2S	• foul smelling type gas • rotten egg type • anaerobic biological decay process in land, marsh, ocean • from craft pulp industry
mercaptan	• strong odour { is in LPG } • pulp mill, Refinery, chemical manufacturing plant
SO_2	• from combustion of coal • Refinery, chemical plant, incineration plant
HF	• Pottery • Brick Plant • Aluminium Industry • phosphate fertilizers

Imp.



Photochemical smog constituent $\begin{cases} \rightarrow O_3 \\ \rightarrow PAN \\ \rightarrow CO \end{cases}$



major constituent (i) O_3 (ii) PAN (iii) HC

factors affecting (PCS)

- (i) light intensity
- (ii) Hydrocarbon reactivity
- (iii) HC, Nitric oxide
- (iv) Presence of light absorber
- (v) meteorological absorber
- (vi) height and intensity of atm. inversion

effects:- (PCS)

- (i) eye irritation due to aldehyde, PAN
- (ii) vegetation damage due to O_3/NO_2 ~~LEAN~~
- (iii) visibility reduction
- (iv) cracking of rubber
- (v) fading of dyes.

Photochemical oxidant effects

- (i) Cause coughing
- (ii) Shortness of Breathe
- (iii) Headache.

effect of air pollution on human :-

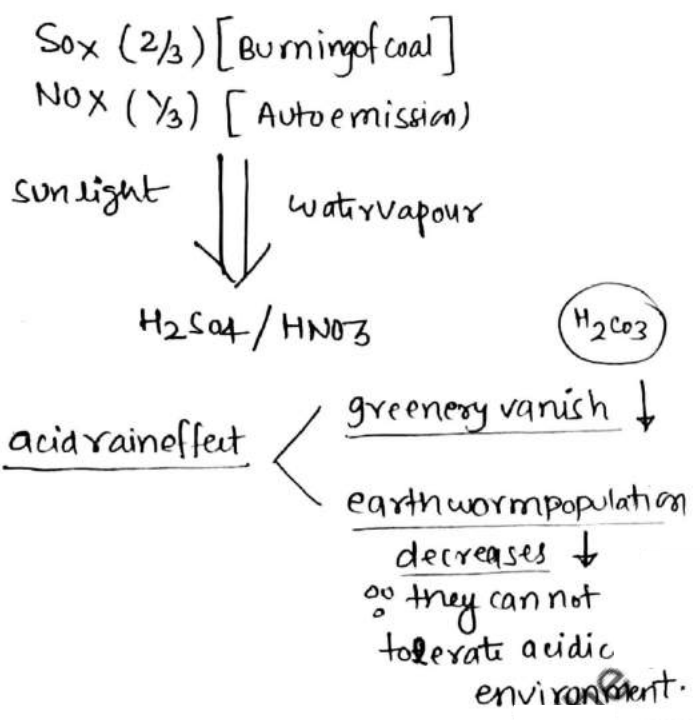
- | | |
|--|--|
| (i) SO_2 | <ul style="list-style-type: none"> • affect <u>mucous membrane</u> • bronchial <u>spasm</u> $\rightarrow$ swelling • Asthma patient badly affected |
| (ii) CO | <ul style="list-style-type: none"> • affect <u>central nerve system (CNS)</u> • great affinity for combine with <u>hemoglobin</u> to form <u>COHb</u> hence it reduce ability of hemoglobin to carry O_2 to body tissue. |
| (iii) NO_x
$\swarrow \searrow$
NO NO_2
<small>nitric oxide nitrogen oxide</small> | <ul style="list-style-type: none"> • eye & nasal irritation • pulmonary discomfort. |
| (iv) H_2S | <ul style="list-style-type: none"> • rotten egg type smell • exposure for short period can result into fatigue of sense of smell |
| (v) Ozone | • <u>Harmful respiratory system</u> than SO_x |
| (vi) fluoride | • Fluorine cumulative poison ($H_2F \rightarrow$ less harmful) |
| (vii) Lead | Source $\rightarrow$ automobile
<ul style="list-style-type: none"> • <u>mental retardness</u> • Abnormality in fertility & pregnancy • <u>liver & kidney damage</u> • <u>gastrointestinal damage</u> |

↑ Exosphere	78% → N_2
Thermosphere	21% → O_2
Mesosphere	1% → Ar
Stratosphere	0.03% → CO_2
Troposphere	Inert

Global warming :-
major greenhouse gases {water vapour}

	Source
CO_2	Burning of fossil fuel, solid waste
CH_4	Anaerobic decay of organic waste
N_2O nitrous oxide	agriculture and industrial activity.
CFC	Refrigerator, AC, paint, spray
SF_6	Insulator, magnesium industry

acid rain (PH < 5.6) :-



Remedy :- neutralize the acid with Lime

- Ozone layer Depletion :- group of CFC's
- Primary Reason → CFC / freons
 - Ozone layer acts as filter for (UV) rays
thus protect against <
 - Burn
 - skin cancer
 - 90% Ozone → Stratosphere (15-50 km)
 - Montreal convention
 → ozone depleting substance ↓
 CFC HFC (ODS)
 - Vienna convention
 → Protection of ozone layer.

Reverberation time — time required to reduce noise by 60dB
 'or'
 time sep. to reduce the intensity to one million of intensity.

TTS (temporary Threshold shift)
 → temporary loss of hearing

PTS → (Permanent Threshold shift)
 → permanent loss of hearing